

DRAFT

John Payne

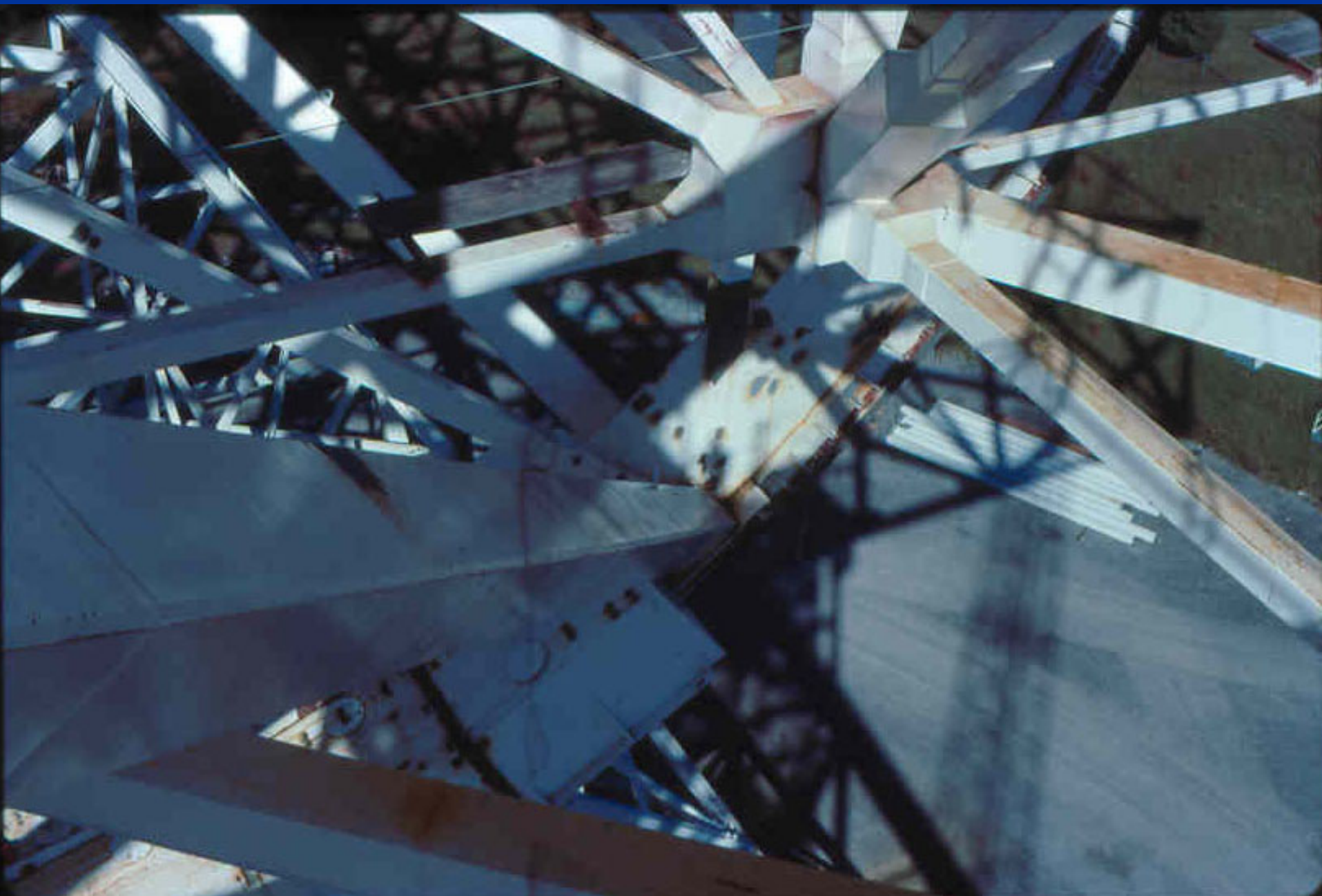
A tribute to the
GBT experimental work

10/26/2006

GBT NATURAL FREQUENCY

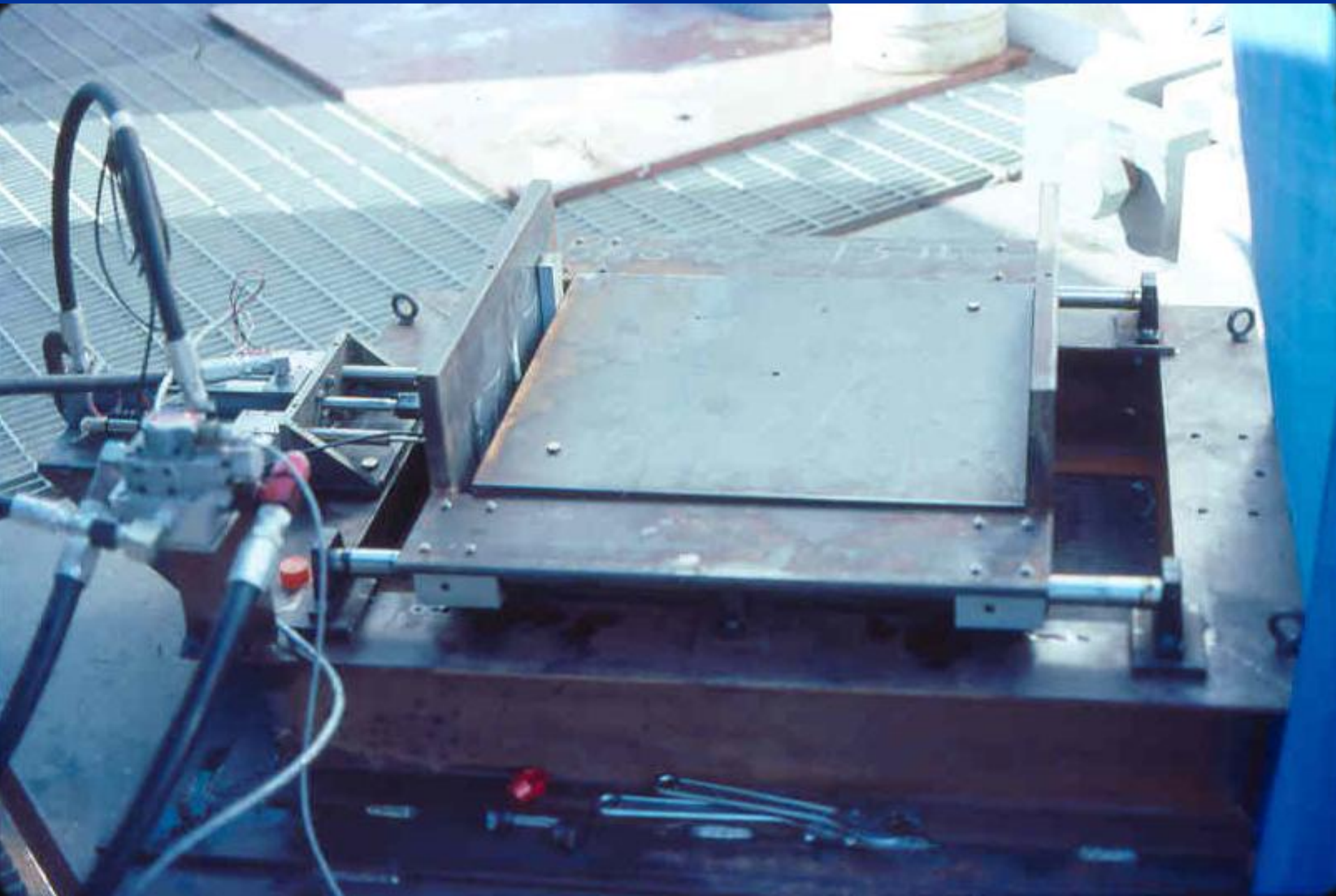








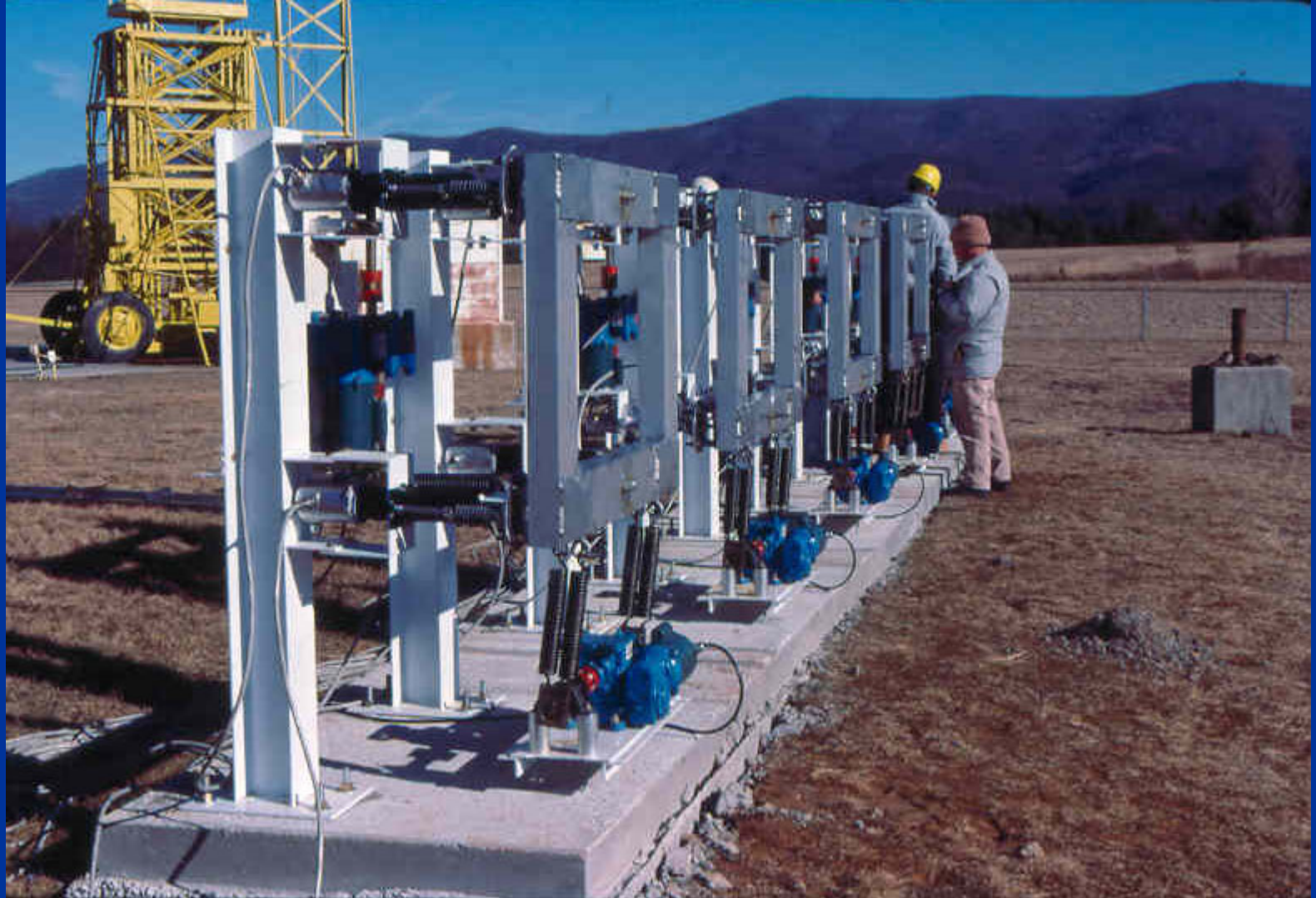






ACTUATORS

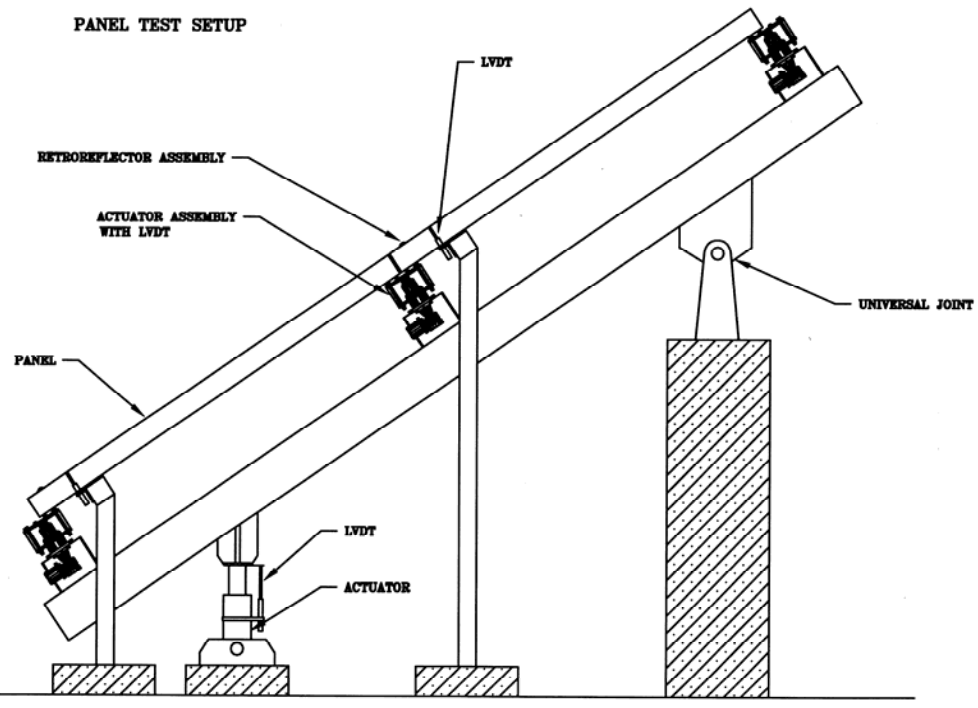






PANELS

PANEL TEST SETUP





NATIONAL RADIO ASTRONOMY OBSERVATORY
Green Bank, West Virginia

MEMORANDUM

August 26, 1992

To: Bob Hall, Lee King
From: J. Payne, D. Parker
Subj: Setting the panels on the GBT

Introduction

The initial setting of the panels on the GBT will consist of setting the panel to panel heights at each actuator. In order to avoid repeated setting of the surface, it is highly desirable that this setting be done just once, with sufficient precision for high frequency operation of the GBT. Due to the fact that we are using the same mold for several tiers of panels, panel edges along a radius will be offset by up to 200 microns. In order not to degrade the overall surface precision, this initial panel to panel setting should be accurate to around 25 microns. In this note we describe a suitable instrument for measuring and recording the relative panel heights at each actuator.

The Instrument

A sketch of the proposed tool is shown in Figure 1.

A shaft, screwed onto the actuator, provides a reference for a jig that slides over the shaft. A step in the shaft permits location of the jig. A tapered shaft (in the manner of a screwdriver blade) fits between the panel gaps in order to locate the jig in rotation around the shaft. Four electronic dial indicators mounted to the jig make contact with the reference points on the panel. A suitable indicator is a Mitutoyo 534-182-1 (data sheet attached). This indicator has a range of 12.7 mm, a resolution of 1 micron, a visible display and an SPC output. The indicator is battery powered, with a battery life of 500 hours. Assuming a separation between the indicators of approximately 15 cm, the angle of the actuator extension shaft with respect to the surface tangent needs to be known to an accuracy of around one arc minute to limit errors in setting to less than 25 microns. Gravity is a convenient reference to use here. In the radial

direction, the angle of the surface tangent with respect to gravity is known for each actuator position. In the circumferencial direction, horizontal is a convenient reference plane.

The accuracy required of the tilt measurement (better than 1 arc minute) precludes the use of a large dynamic range "digital protractor". A suitable inclinometer is manufactured by Schaevitz, a LSRP-14.5, which has a range of ± 14.5 degrees. A series of wedges will be needed to maintain the radial inclinometer within its range for the outer parts of the reflector. This simple option has been chosen over a servo controlled platform which, while more elegant, would be more bulky and complex.

A block diagram illustrating the various components is shown in figure 2. All components are battery operated, and a data sheet on a typical hand-held computer is attached. A convenient (but certainly not necessary) means of identifying each actuator would be a bar code transfer on the reflector surface. The operator would read the bar code after installing the tool. The correct actuator tilts would be stored in the computer, along with the correct digimatic indicator readings. Corrections to these readings would then be computed on the basis of the tilt deviations. A reading for "adjustment screw #1" could then be displayed on the screen. The operator would adjust #1 until the reading is zero and move on to #2. After the setting process is complete, all four digimatic readings are stored, along with the tilt readings to be recovered later in a lab-based PC. It should be noted that with this procedure not only are the panels set with high precision with respect to one another, but the relationship between the corner cube (when installed) and the panels is now known to a high precision. This, theoretically at least, permits the setting of the surface using the laser rangefinders.

One issue that needs to be settled is the deformations resulting from the weight of the operator(s) in the vicinity of the actuator. We can include a "strobe" option that will permit the operator to stand some distance away and remotely initiate readings.

Cost of Tool

Four digimatic indicators (\$350 each)	1400
One inclinometer stack	2400
One hand held computer	1700
One digital/analog interface	500
Miscellaneous	<u>1000</u>
Total	\$7000

We are proceeding with construction of such a tool, and it should be finished in 2 months.

JP/ss

cc: F. Crews
M. Barkley
D. Hogg
J. Lockman

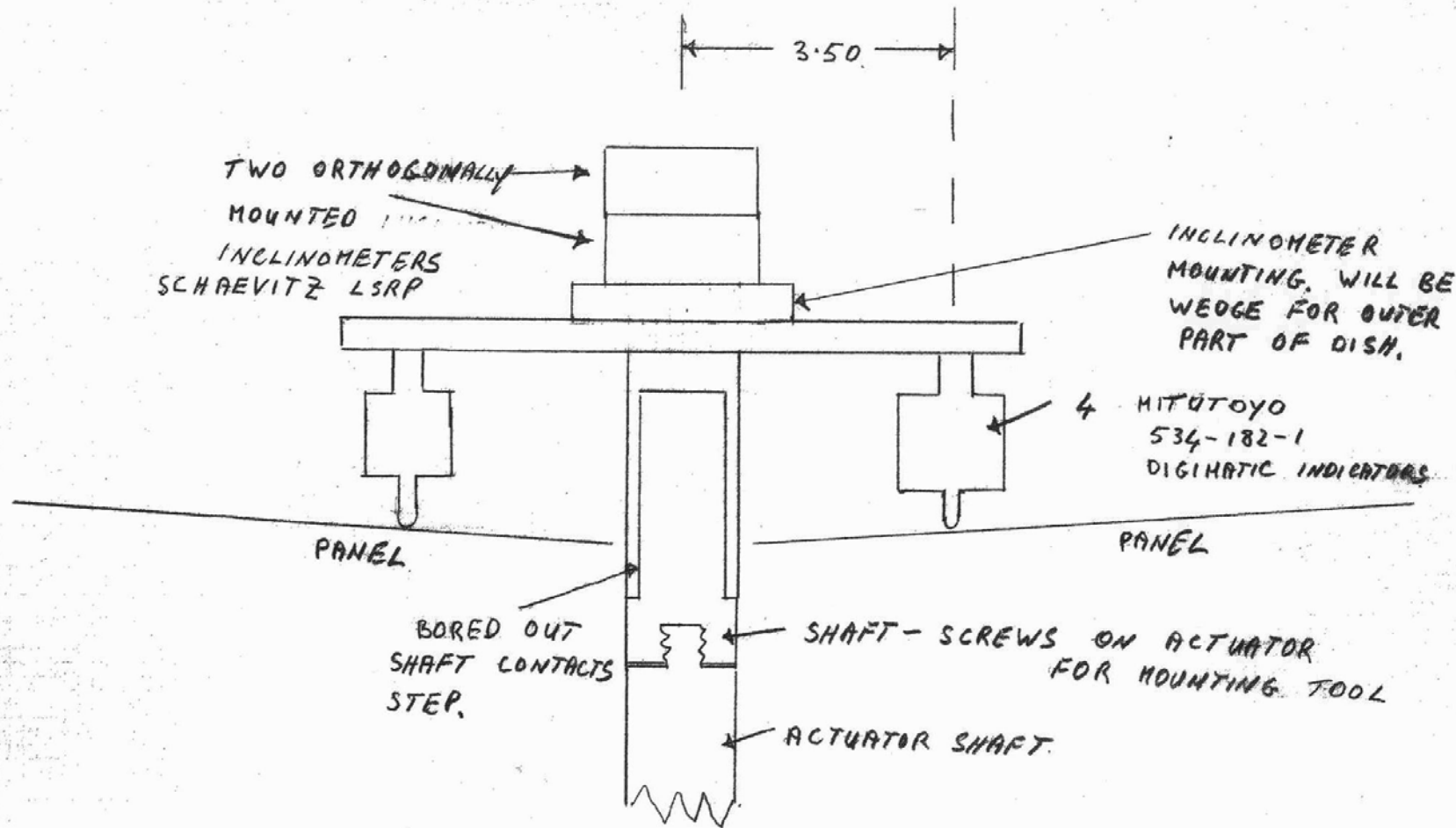


FIG 1 - SKETCH OF TOOL - SIDE VIEW.

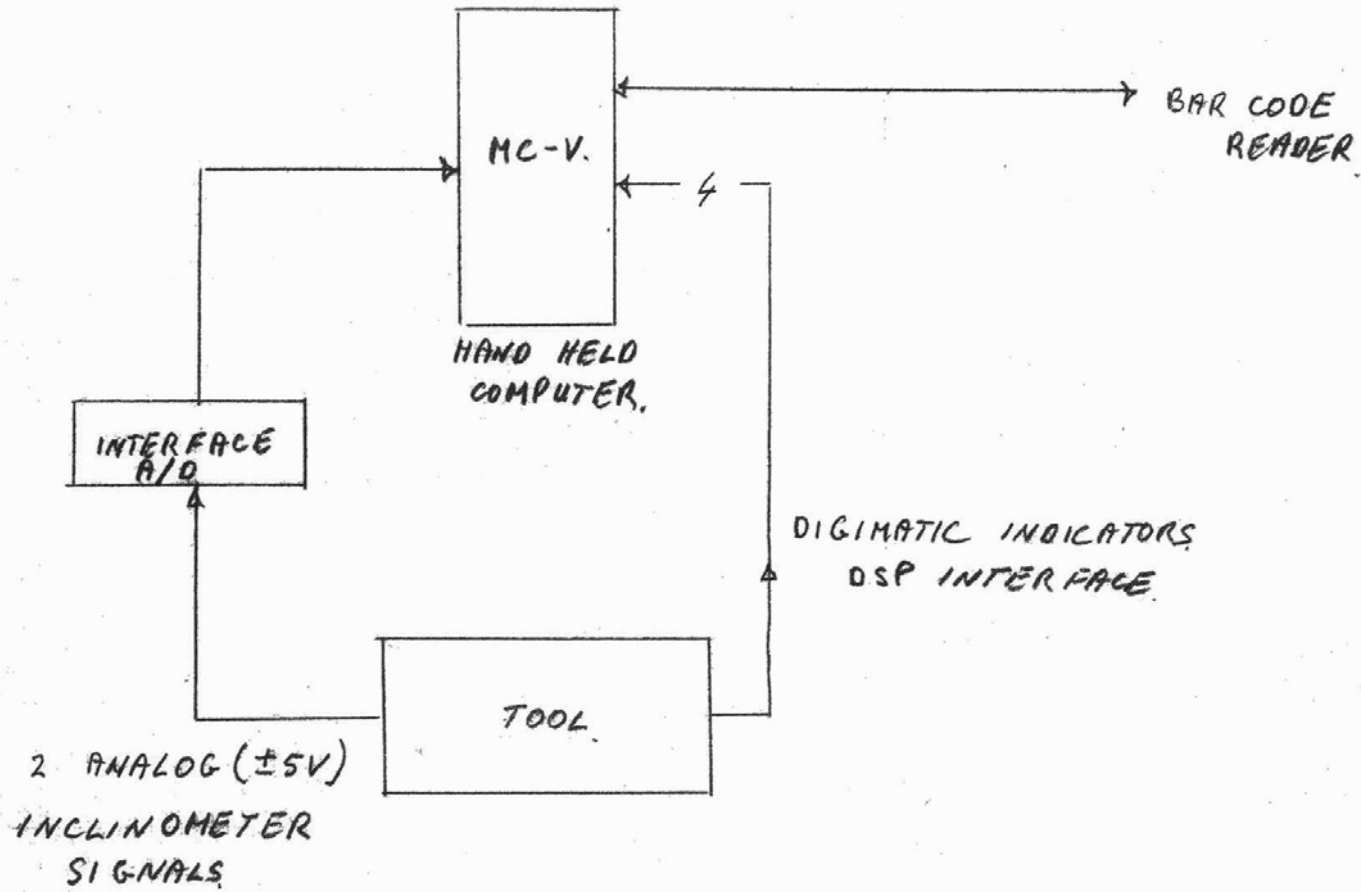
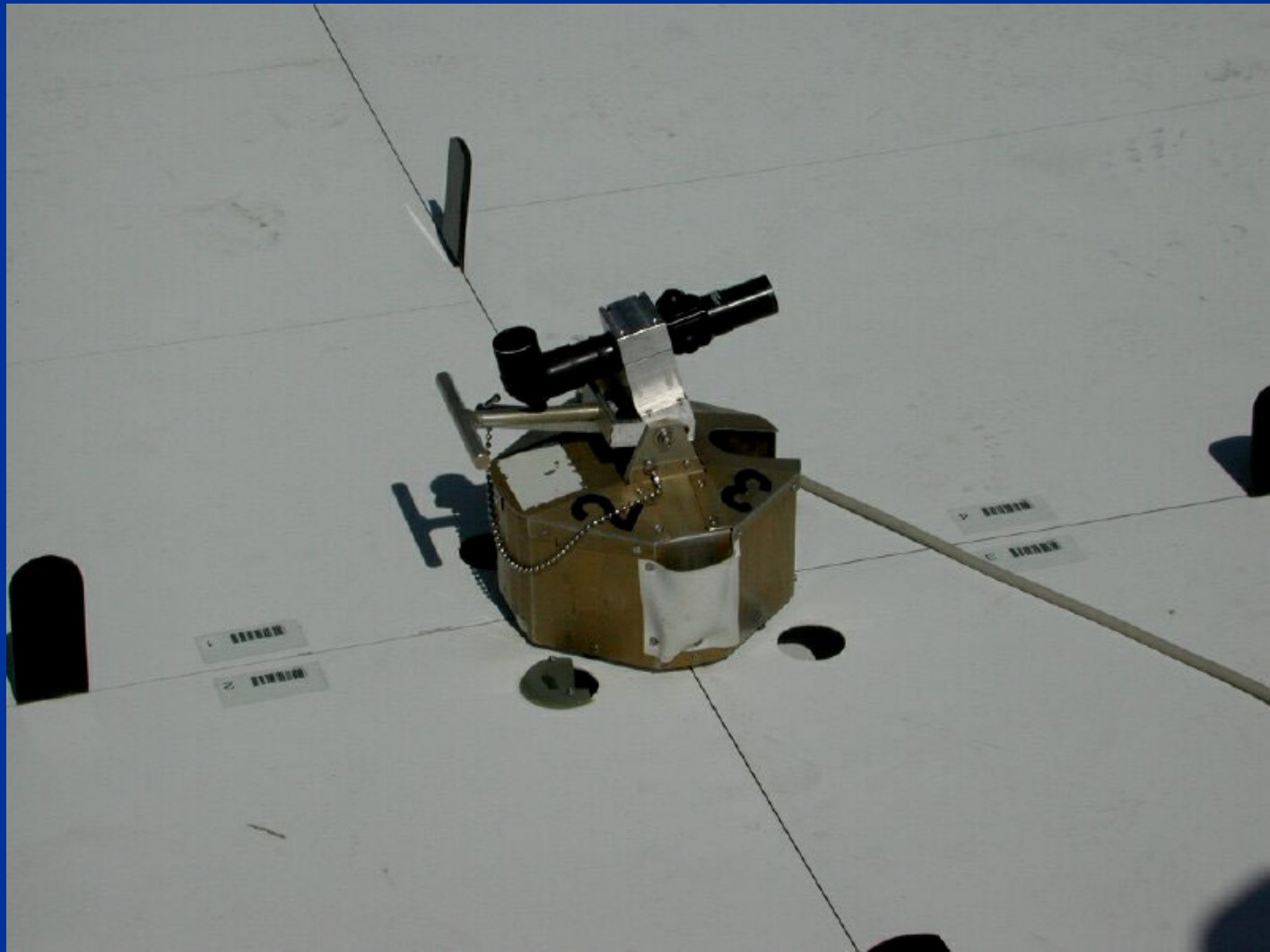


FIG 2 INTER CONNECTIONS



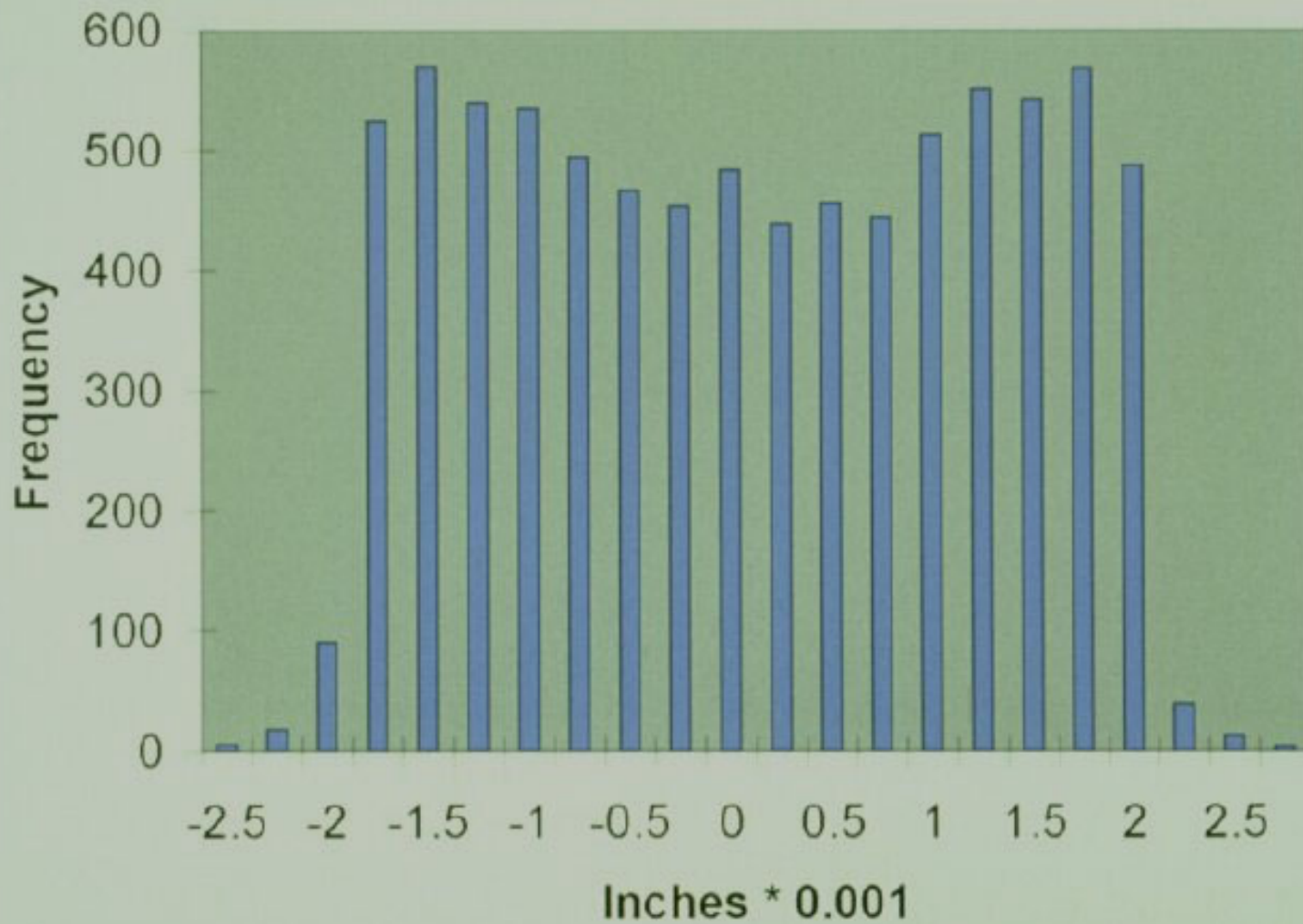








Corner Setting Mid-Range Results



HYDROSTATIC LEVEL





140 FOOT EXPERIMENT





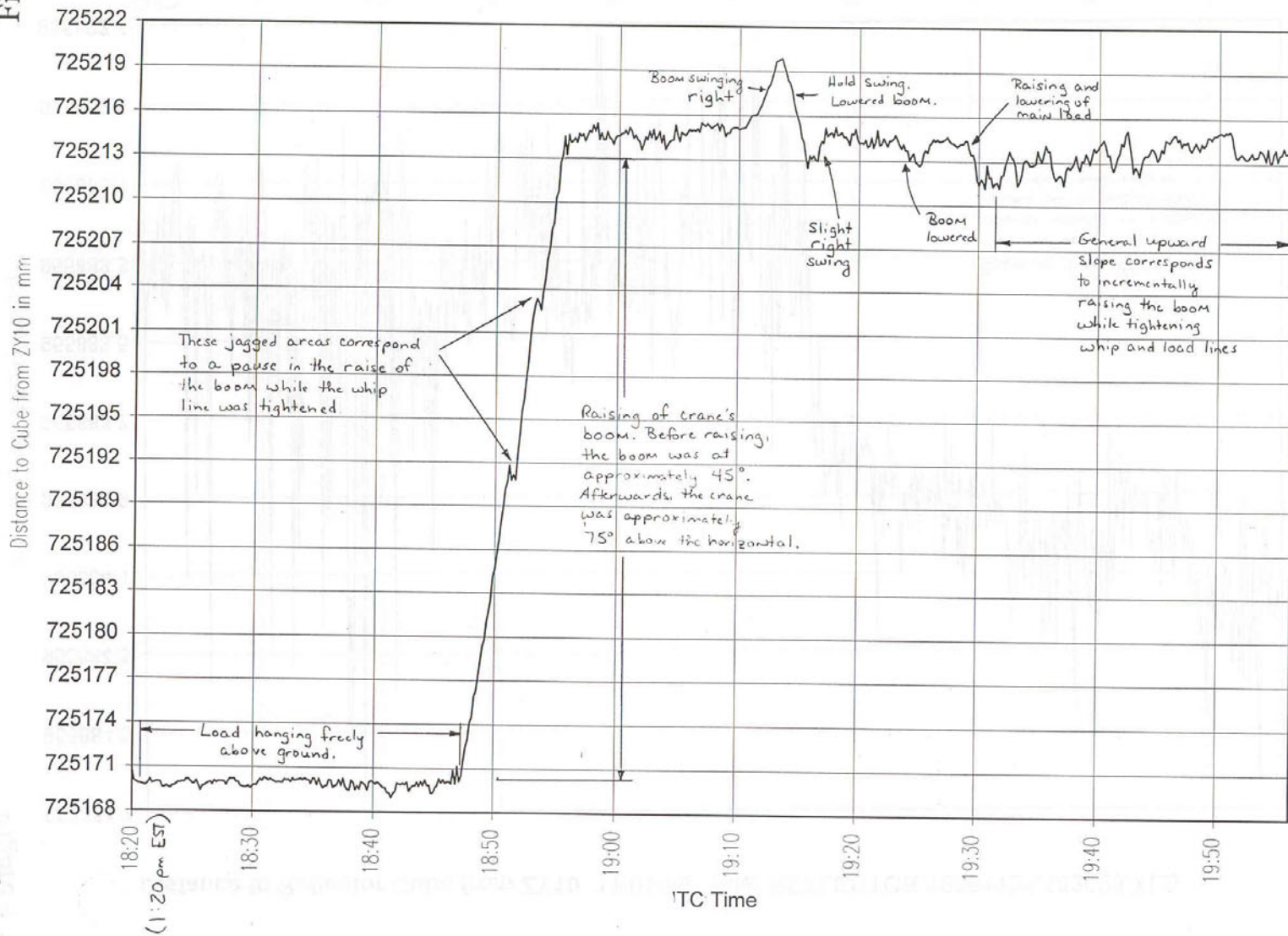


DERICK DEFLECTION



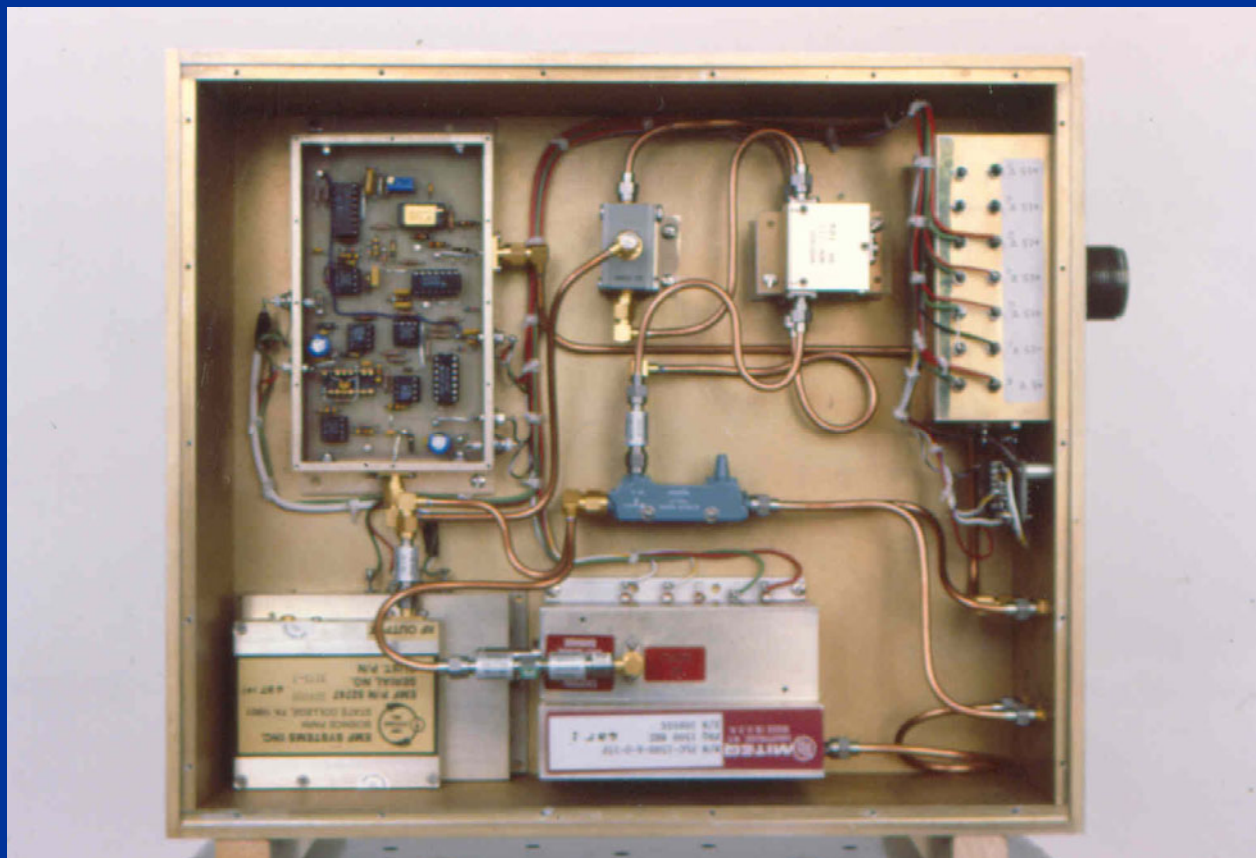


Figure 3

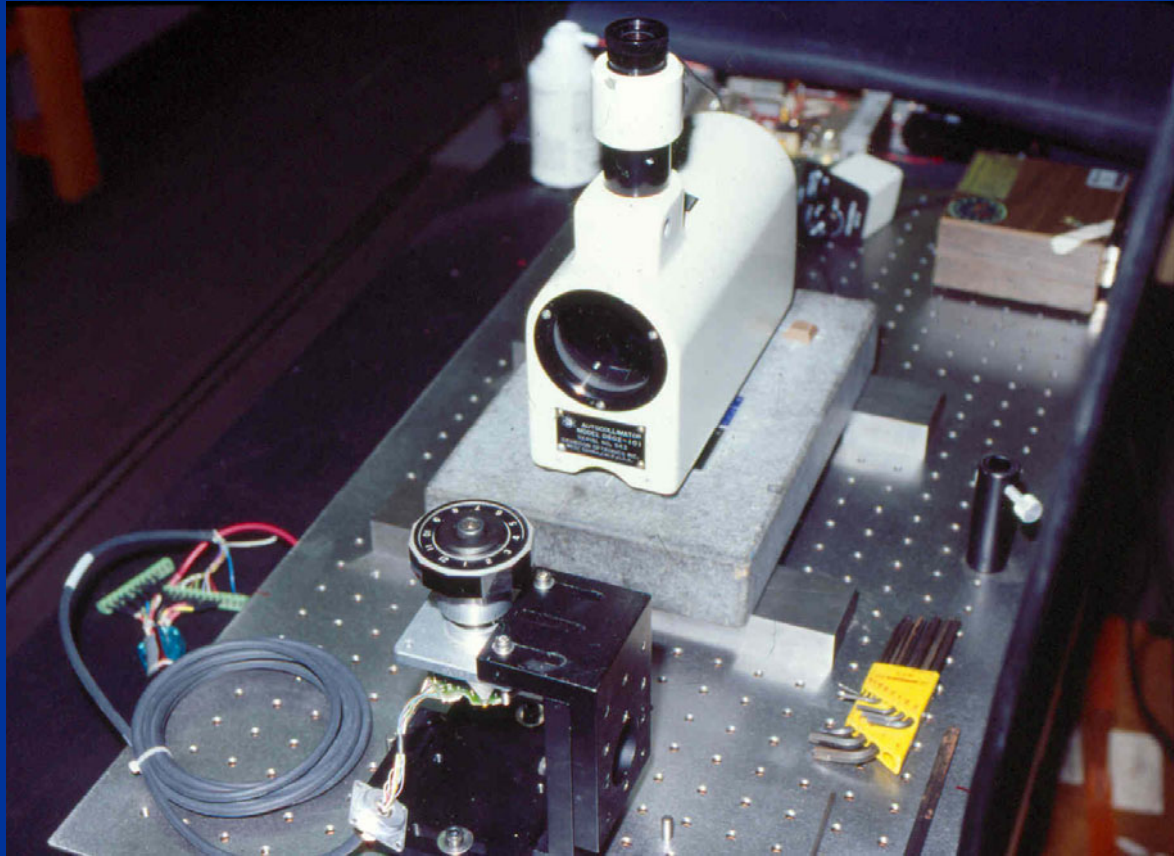


OSCILLATORS





METROLOGY LAB

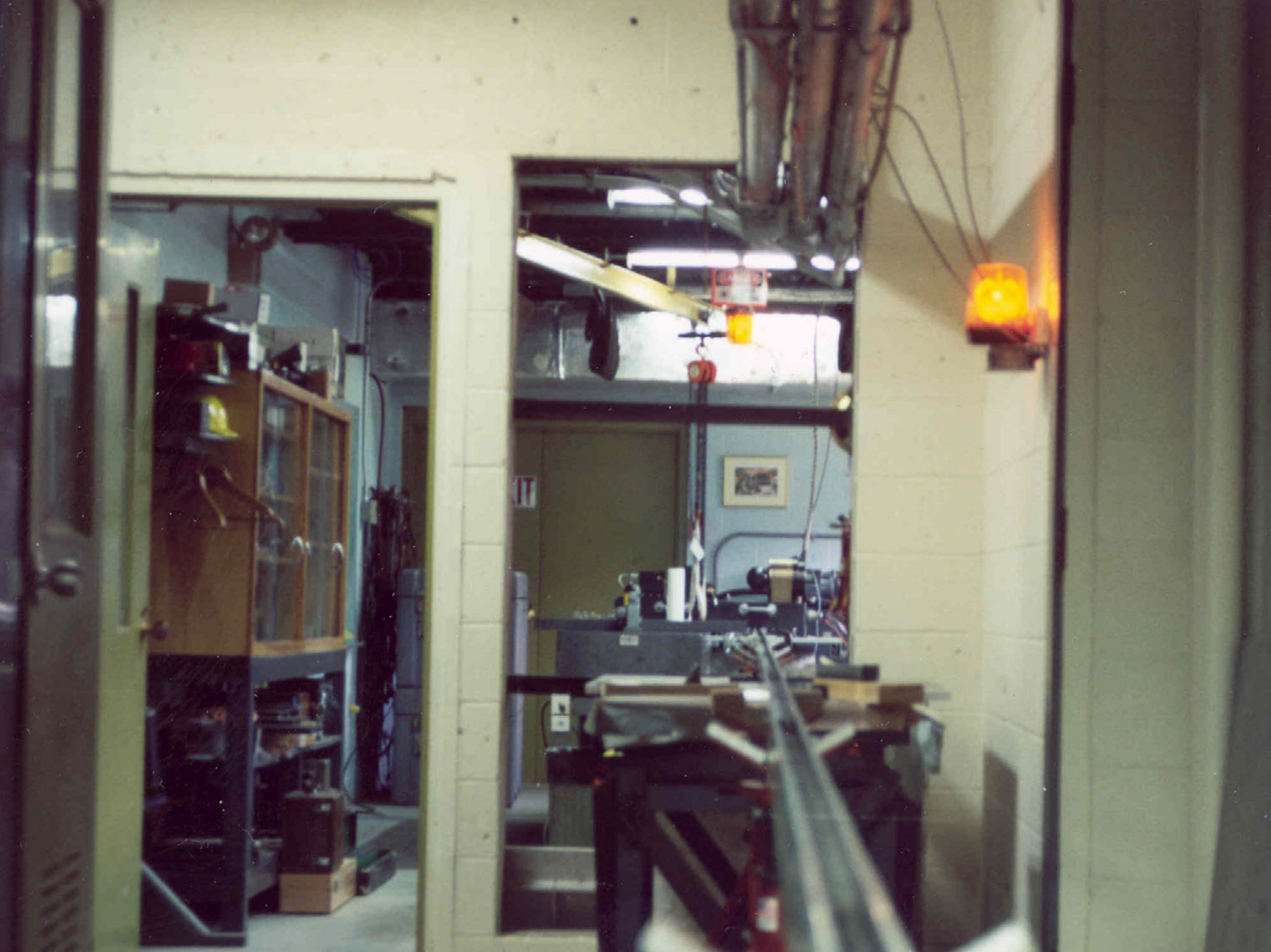




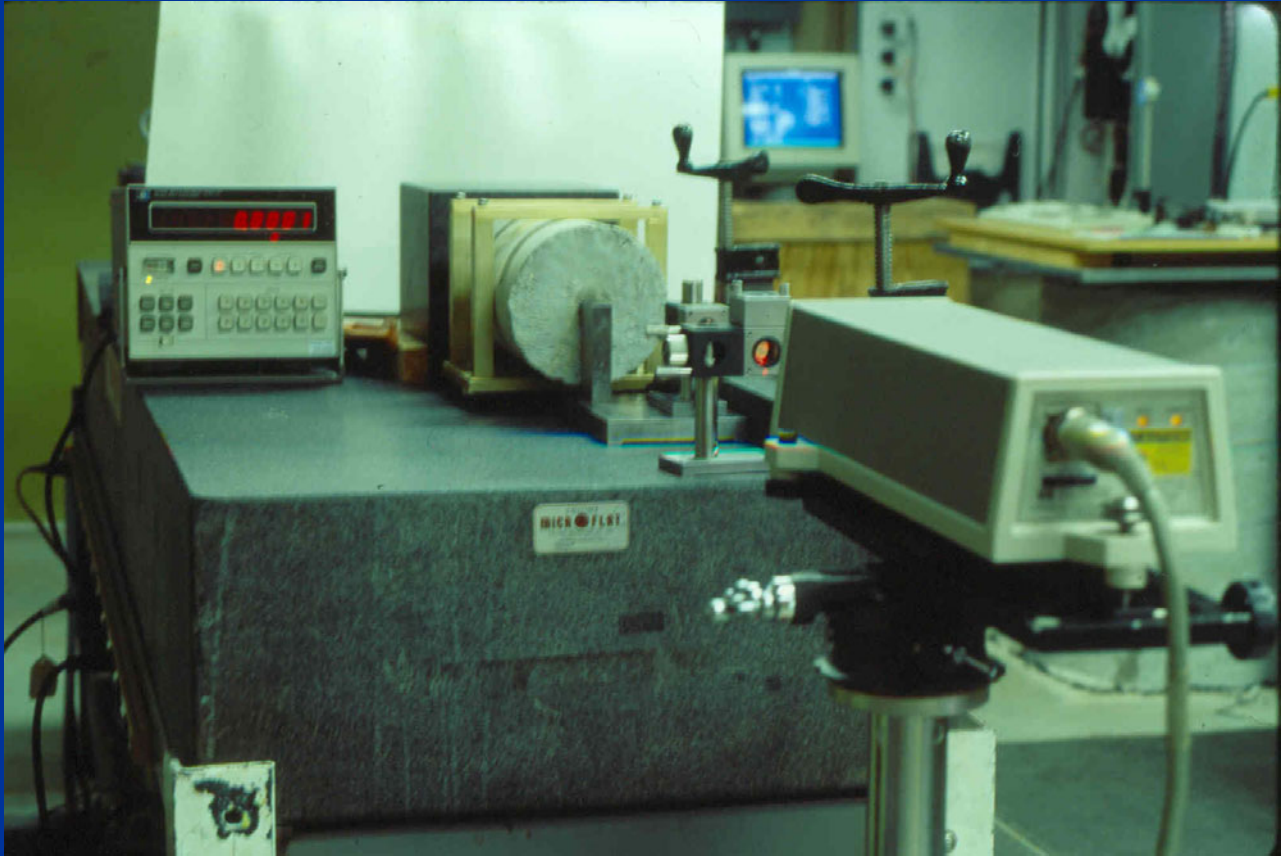
Mitutoyo

CDI
DIGITAL DEPTH INDICATOR
SERIAL NO. 111 24
PART NO. 111 24
MADE IN JAPAN

93 8 5







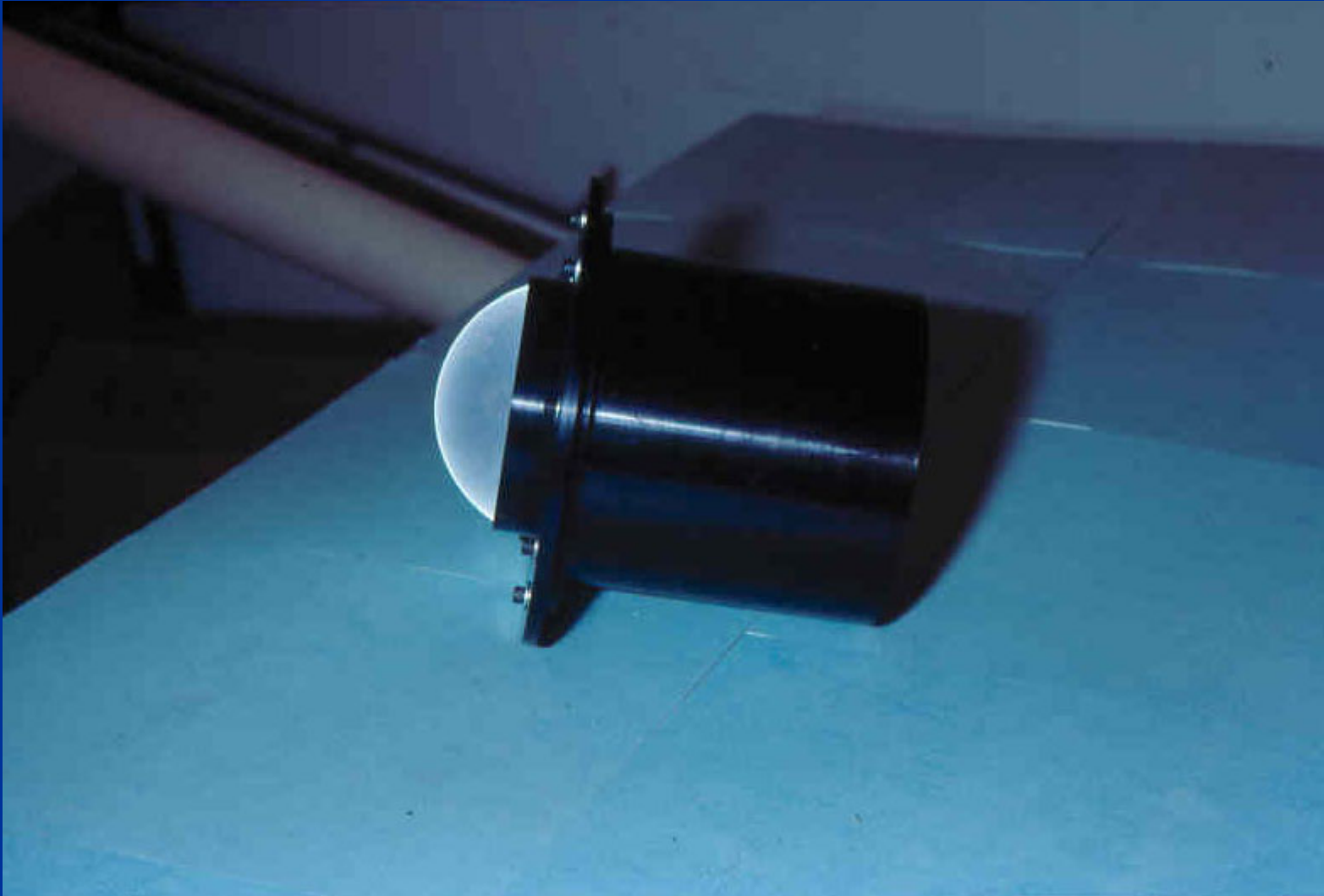
GeoSAR







RETROREFLECTORS







AUTOCOLLIMATOR



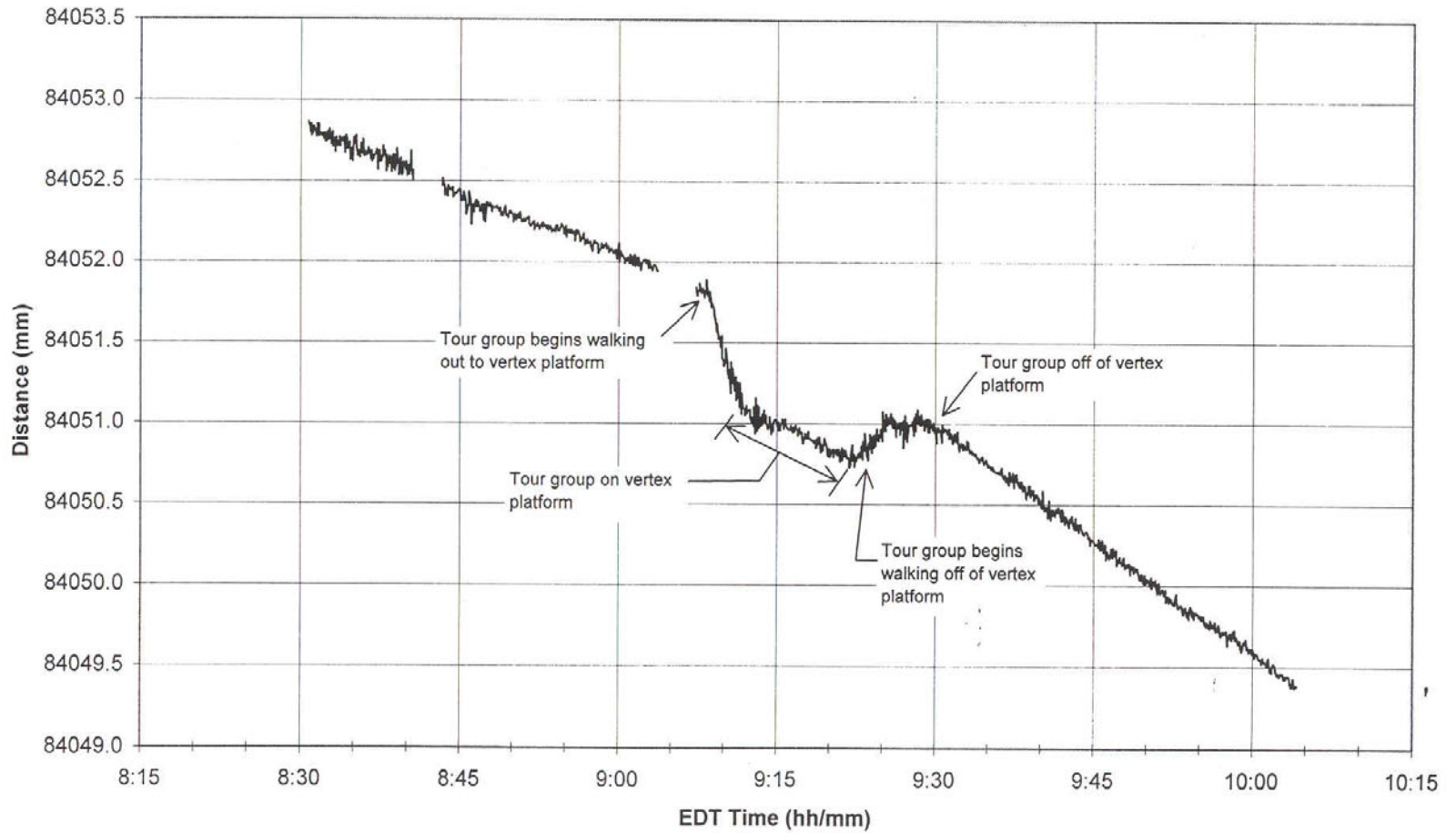




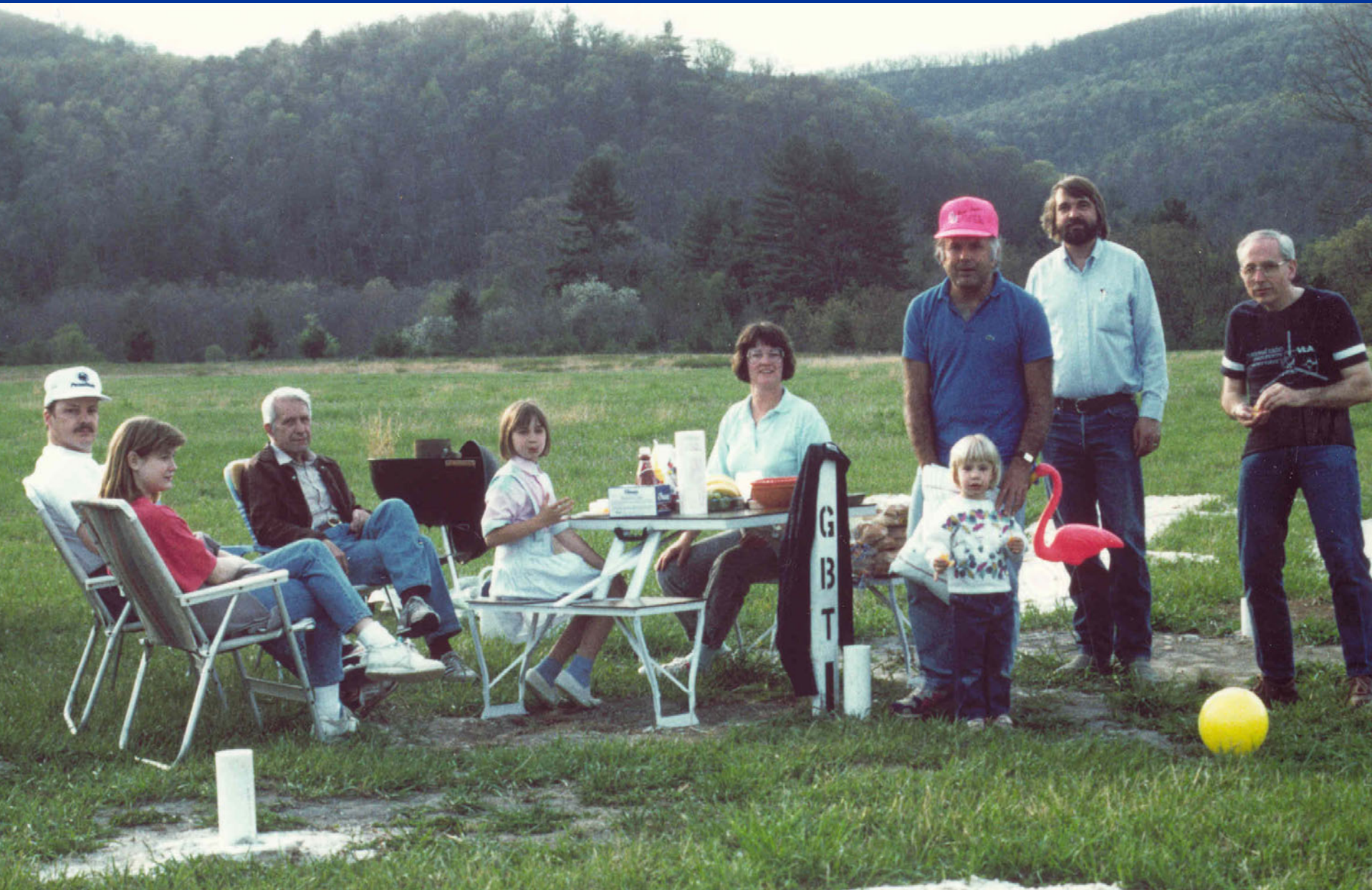
HORIZONTAL FEED ARM
DEFLECTION BY ADVISORY
COMMITTEE

Distance to ZEG31020 vs Time, ZY111 10/17/98

File: ZEG31020.experiment.xls Disk: B234



METROLOGY GROUP

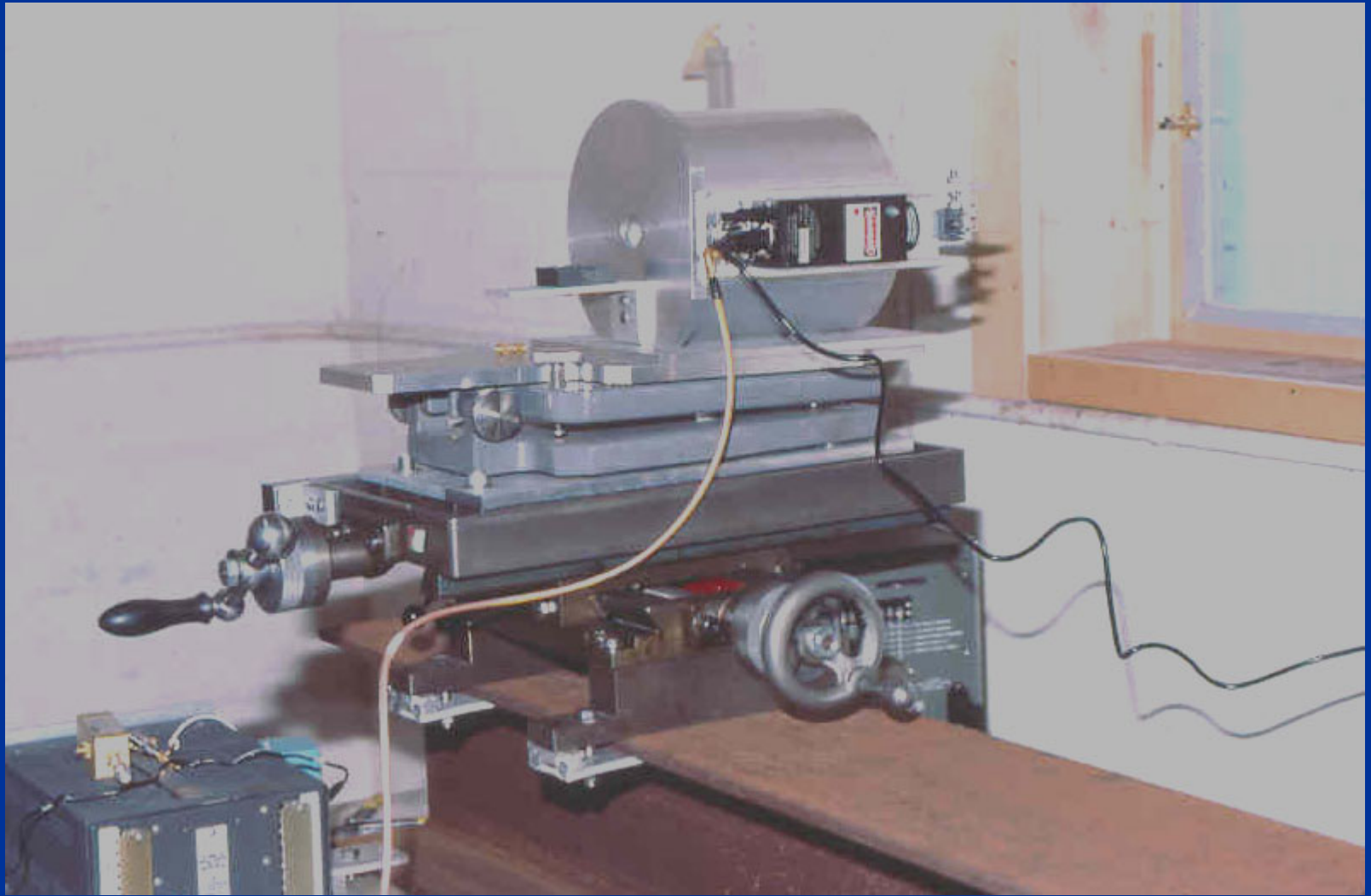




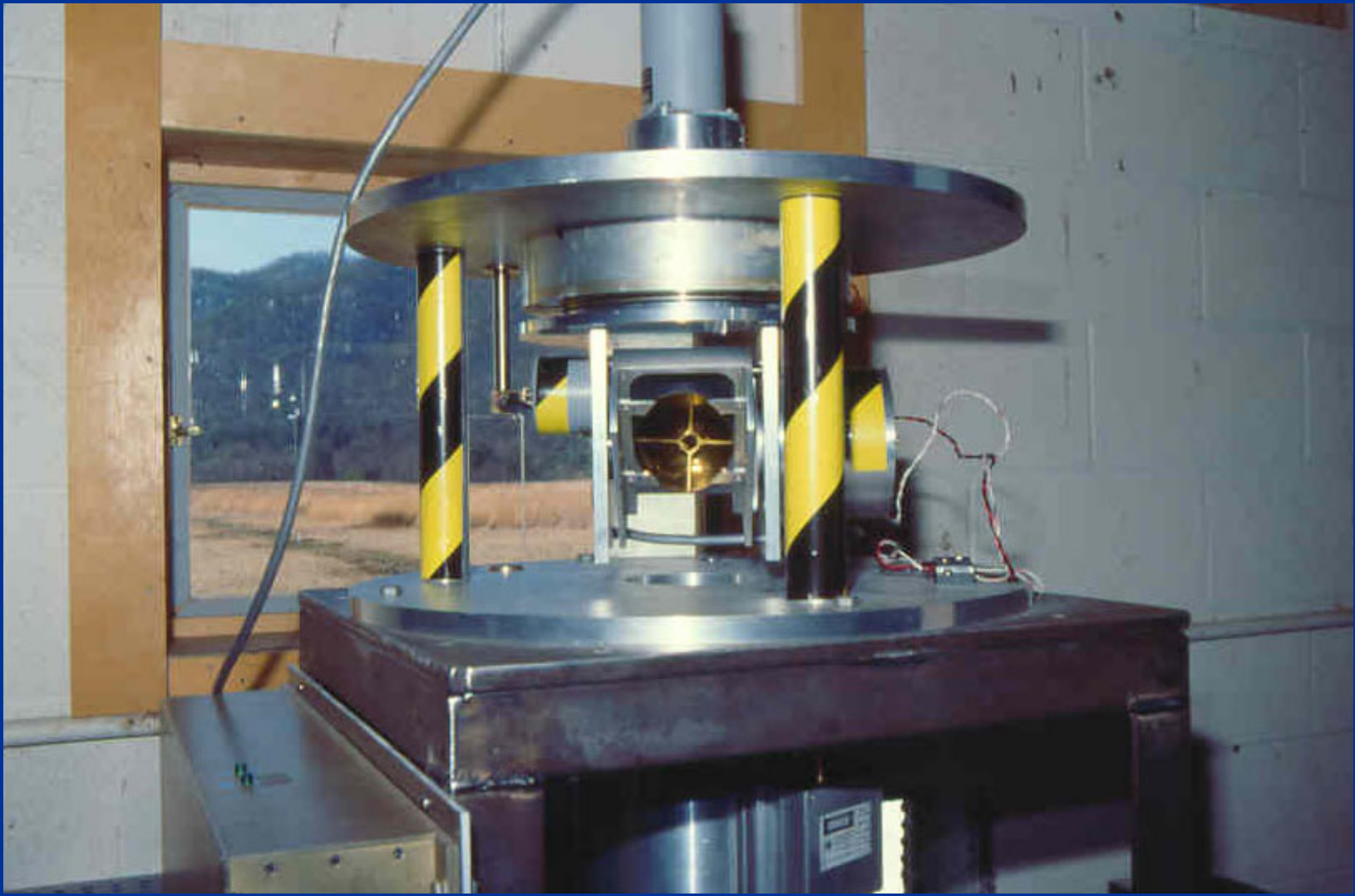
RANGER R&D

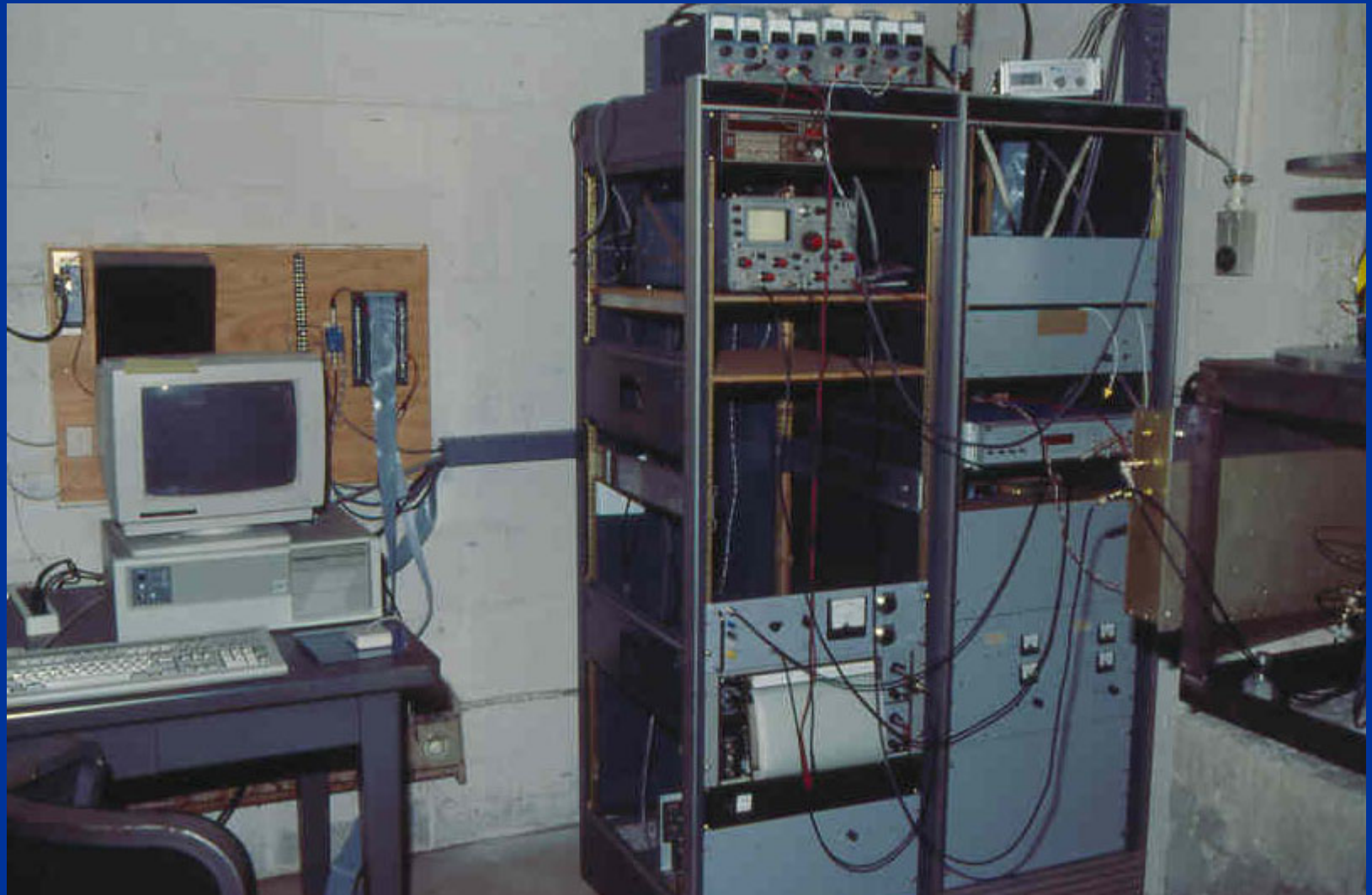






















US005455670A

United States Patent [19]

[11] Patent Number: 5,455,670

Payne et al.

[45] Date of Patent: Oct. 3, 1995

[54] OPTICAL ELECTRONIC DISTANCE MEASURING APPARATUS WITH MOVABLE MIRROR

[75] Inventors: John M. Payne, Tucson, Ariz.; David H. Parker, Arbovale, W. Va.; Richard F. Bradley, Stanardsville, Va.

[73] Assignee: Associated Universities, Inc., Washington, D.C.

[21] Appl. No. 68,543

[22] Filed May 27, 1993

[51] Int. Cl.⁸ G01C 3/08; G01C 3/00; G01B 11/26; G01B 11/24

[52] U.S. Cl. 356/8.1; 356/3.11; 356/141.1; 356/152.2; 356/152.3; 356/376; 356/2

[58] Field of Search 356/1, 4, 5, 141.1, 356/152.2, 152.3, 376, 3.11, 5.1, 2

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J. M. Payne et al.; Rev. of Scientific Instr.; vol. 63, #6; Jun. 1992; p. 3311.

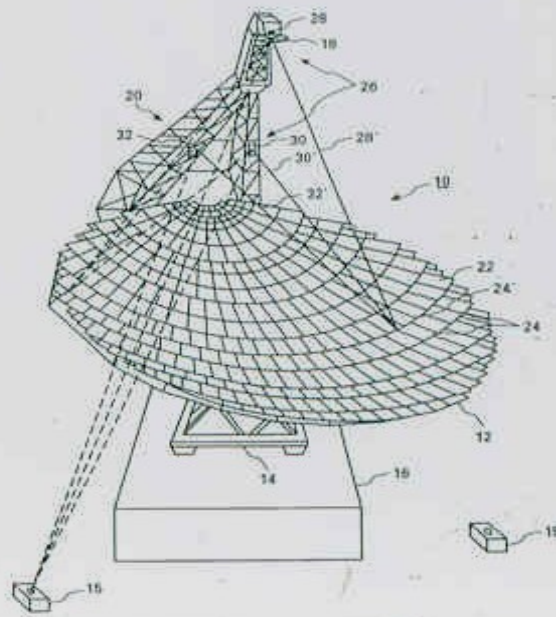
Primary Examiner—Stephen C. Buczinski

Attorney, Agent, or Firm—Margaret C. Bogosian

[57] ABSTRACT

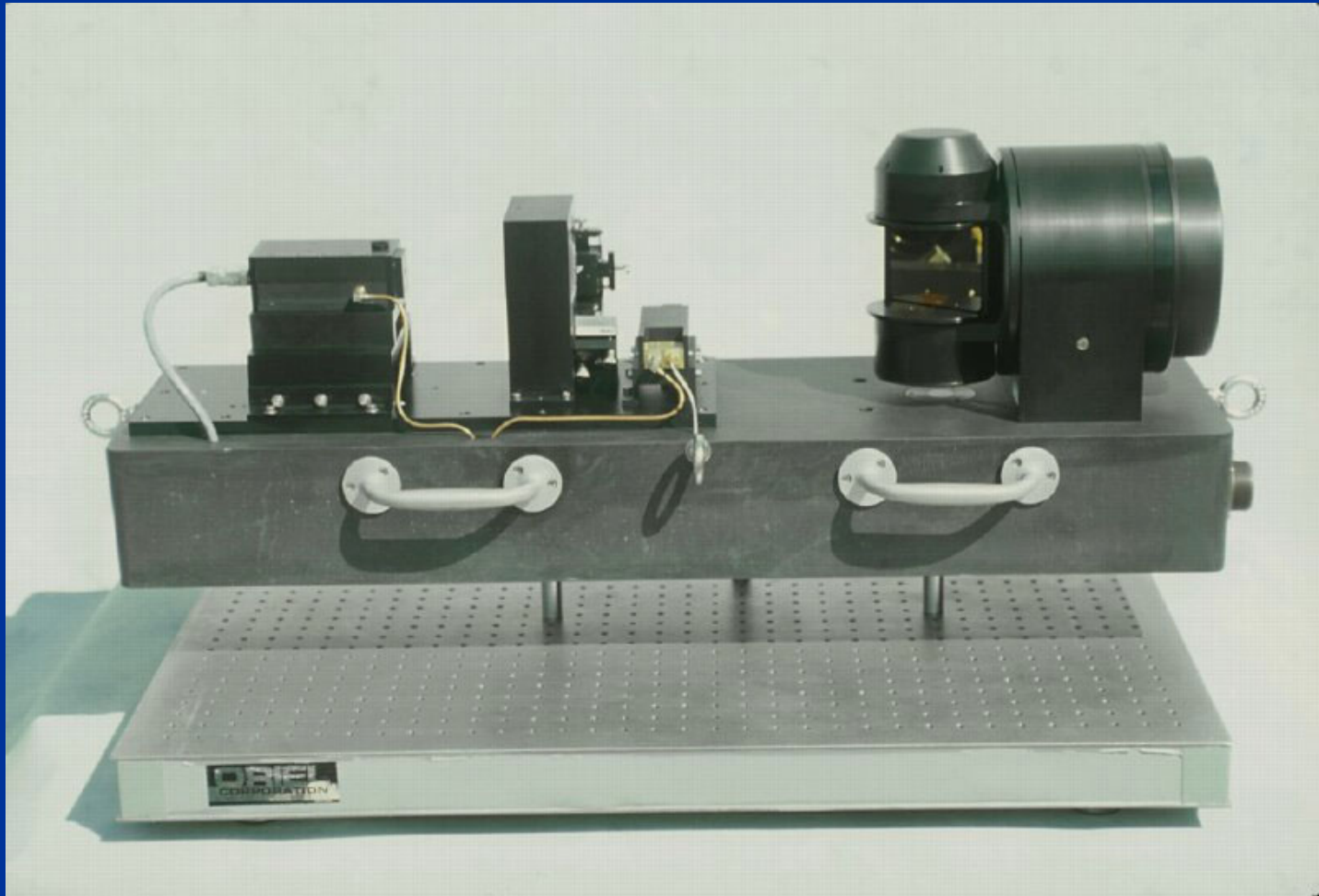
A rangefinder system employs three laser rangefinders for determining three dimensional coordinates, each rangefinder using a steerable mirror for aiming the rangefinder beams at a series of retroreflectors. The beams are modulated at 1.5 GHz. The system includes a signal at an offset frequency of 1 kHz for phase detection. A digital phase detector under control of a local computer, as is the mirror, computes phase difference which is used to measure the distances to the retroreflectors. Correction is made for zero point phase drift of the circuit of each rangefinder and a benchmark reference to a distant retroreflector corrects for atmospheric effects on the measurements. A central computer directs the implementation of the tasks of the local computers of each rangefinder and computes and displays trilateration computation results made from the three rangefinders. The system can measure the distance to five different points per second with ranges up to 120 m at an accuracy of about 50 μ m.

32 Claims, 14 Drawing Sheets



RANGER CONSTRUCTION





SUBREFLECTOR



Other areas of interest

- Servo/stiction
- Performance measurement program
- Powder paint deformations
- Active damper for feed arm
- Quadrant detector
- Holography problems
- Tertiary mirror
- Wheel taper measurements