

13/6/57

Overall Performance

Input dial 8, Revolver dial 10

Tuner to mark, BFO 87

Attenuator 6DB, B+ 140V Bias +6.0V

Stage	R.F.	Mix	I.F.	I.F.	6KC band
Cathode	3.2V	1.1V	2.7V	3.0V	25Ω dummy antenna
Color	clear	brown	blue	white	

Velocity potential 0.25 volt 100,000Ω load

2 Volts Output.

No signal Beat Oscillator
Output 1.8 volts

Freq. KC	Input mV
143	15
144	1.15
145	0.6
146	0.55
147	0.50 ← zero
148	0.55 beat.
149	0.6
150	0.7
151	2.0
152	45

R.F. noise 0.38 volt
(.13V above diode w/pot)

1²⁵/₃₂" from inside edge
of label to plate to
outside aluminum can

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Input
for 2Vout

Antenna	Rev.	Freq	Input for 2Vout	Notes
3	0	143.5 KC	1.91uv	} 15Ω dummy antenna 24DB attenuator 6 KC band
14	20	154	1.25uv	
33	45	171	1.20	
58	70	186.5	1.1	
96	100	205 KC	1.0	

B+ = 140V Bias = + 5.9V

Cathode to bias

RF + 3.55V Max +0.70V 1st +3.30V 2nd. +3.40V
+2.6V

When distance down to $\frac{3}{32}$ " the noise drops from
when off resonance
2.20V to 0.4V when on resonance.

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Note

All this noise was in the
double diode clipper on first grid.
When this removed the noise is
negligible.

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Antenna Input Performance

Added 46 turns to bottom end antenna input coil making a total of 311 turns. Also rewound primary as 14 turns .032" wire over bottom end of input coil with edges of coils in same plane. Now when input coil tuned above resonance noise drops from 2.90 to 1.2 volt with attenuator at 65B. 25- Ω dummy antenna used. 1 1/16" between black bobble plate and aluminium can. Less than 0.25 volts noise left when input grid is shorted.

Input Coil assembly performance

Freq KC	Primary Open		25- Ω dummy		ratio
	C	Q	C	Q	
145	495.5	100	465?	8?	1.045
180	281	125	302	6?	1.075
220	187.5	139	204	5?	1.080
290	106.5	151	118	5?	1.108

When dist over 1 1/16" there output drops from 2.5V off resonance to 0.6V on resonance
still too loose

(over)

When primary closed by 25- Ω dummy the inductance dropped about 8% and Q to less than 5%. However the coupling between input + secondary still too small.

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Overall Performance. RF System

Input 15 Ω dummy
2.0 volts output

Output Mixer Grid return
1 megohm load.

ant. Dial	set Dial	Freq. KHz	Input mV
91	100	199.5	1.65
Gain	61.6 DB	200.8	1.55
Dip	0.5 DB	203.0	1.65
Peaks	5.0 KC	205.8	1.55
		206.8	1.65

Filament code
R.F. = clear
Mixer = brown
1st I.F. = blue
2nd I.F. = white

31	45	166.0	2.3
Gain	58.8 DB	167.0	1.9
Dip	1.6 DB	170.0	2.3
Peaks	6.8 KC	173.8	1.9
		174.8	2.3

1	0	139.3	3.1
Gain	76.2 DB	140.3	2.3
Dip	2.6 DB	144.0	3.1
Peaks	7.0 KC	147.3	3.1
		148.2	3.1

REVERSE TRANSDUCER
(1) (2) (3) (4) (5) (6) (7) (8) (9) (10) (11) (12)
List of

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R.F. Performance, R.F. stage only

Input R.F. Grid. Output Max. Grid return
2.0 Output volts 1 megohm load

Dial	Freq	Input
100	198.6	36mv
Gain	200.0	33
55.5X	203.0	36.
	205.8	33
	207.0	36

45	165.0	49
Gain	166.5	37.5
	170	49
41.8X	173.5	37.5
	175.0	49

0	138.3	61
Gain	140.0	40
32.8X	144.0	61
	147.7	40
	148.6	61

Put 160K Ω across secondary

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Input Mixer Grid, 10,000 Ω load.
 Input 0.10 volts constant. No Oscillator

π Network

This is Best

Freq KC	Output Volts
85	.13
150	.17
200	.23
230	.332
240	.387
245	.408
250	.412
255	.392
260	.352
280	.177
300	.089
320	.048

Gain
12.3DB
27DB

Gain \rightarrow
10.3DB

Dial	Acc Volts
0	.195
20	.158
40	.120
60	.090
80	.066
100	.053

Transformer

Freq KC	Output Volts.
150	.046
180	.073
200	.108
220	.168
230	.223
240	.290
245	.317
250	.328
255	.316
260	.288
280	.184
300	.134

.32DB

Dial	Acc Volts
0	1.50
20	1.43
40	1.34
60	1.25
80	1.19
100	1.15

30/9/56

Changed Pri. shunt to 330K Ω

Now primary looks into

$$\frac{1}{\frac{1}{33} + \frac{1}{6}} = \frac{1}{4.67} = 214K\Omega$$

This reflected back by ratio of $(4.2)^2 = 17.8$ gives

$$\frac{214}{17.8} = 12K\Omega \text{ into filter,}$$

Resonance still at 250.0 KC.

Thru gives 1.05 volts

$$\text{Gain} = 1.05/0.77 = 13.6 \text{ times}$$

3DB points 236 + 266 KC = 30 KC.

$$Q = \frac{250}{30} = 8.3$$

5 pF goes from 250 to 231 KC.

$$\left(\frac{x+5}{x}\right)^{1/2} = \frac{250}{231} \quad 53200x + \frac{266000}{53210x} = 62300x$$

$$x = \frac{266000}{9300} = 28.6 \mu\text{F}$$

circuit capacity

30/9/56

Characteristics of H. 5000 Output transformer

Pri. 286T .015" dia wire

Sec. 56T .034" dia litz
(8 layers of 7 turns) of litz about 6 1/2 ft

Pri. only

Sec. only

(Core open)

(Pri. open)

outside and high

Freq. Cap. Q

Freq. Cap. Q

55KC 459 123

215KC 445 18

80KC 209 80

250KC 213 5

110KC 100 54

265KC 123 2

120KC 80 49

Not able to go
higher in frequency
as primary
resonates somewhere
just above 250KC

160KC

170KC 30.2 26

$$C_0 = \frac{459}{400} = 3.59$$

20 ft.

Two gaps each .020" one at
each end of primary coil.
(6000)

30/9/56

Primary reduced to 236 Turns

Now Resonance 257KC

3DB points at 246 + 263KC

3DB band 17KC

77mw input gives 1.86v output

$$\text{Gain} = \frac{1.86}{.077} = 24.2 \text{ times}$$

added 5pf + 470K Ω across pri,
Resonance now, 231KC

77mw gives 1.18V olts

$$\text{Gain} = \frac{1.18}{.077} = 15.3 \text{ times}$$

3DB, 220 + 243KC = 23KC

Took off 5pf, Now 470K Ω only

Resonance 250.0KC


77mw gives 1.20 volts

SANDY BAY, HOBART
AUSTRALIAN NATIONAL HOTELS LTD.
PROPRIETORS:

WEST POINT RIVIERA HOTEL

3DB 237 + 263KC = 26KC

TELEPHONE: 9516 (4 LINES)

Ratio now $\frac{236}{56} = 4.21$ Pri.  should look into 180K Ω

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Mixer Output Transformer

Secondary of mixer assembly

Freq	C	Q	Equation
240 kc	431	29	$L(C_1 + C_0)\omega_1^2 = L(C_2 + C_0)\omega_2^2$ $C_1\omega_1^2 + C_0\omega_1^2 = C_2\omega_2^2 + C_0\omega_2^2$
270	284	21	$C_0(\omega_2^2 - \omega_1^2) = C_1\omega_1^2 - C_2\omega_2^2$
300	180	12	$C_0 = \frac{C_1\omega_1^2 + C_2\omega_2^2}{\omega_2^2 - \omega_1^2}$
320	120	8	$\omega_2 = \frac{4}{3}\omega_1, \text{ so } \omega_2^2 = \frac{16}{9}\omega_1^2$
340	70	5	$C_0 = \frac{C_1\omega_1^2 - C_2\frac{16}{9}\omega_1^2}{\frac{16}{9}\omega_1^2 - \omega_1^2} = \frac{C_1 - \frac{16}{9}C_2}{\frac{16}{9} - 1}$

$C_0 = \frac{431 - \frac{16}{9}120}{\frac{7}{9}} = (431 - 213) \frac{9}{7} = 280 \text{ pf}$. This is due to removal of primary.

Same but primary removed,

Freq	C	Q	Equation
285 kc	450	183	$C_0 = \frac{450 - 396}{3} = \frac{54}{3} = 17 \text{ pf}$
350	291	140	$L_0 = \frac{1}{(6.28 \cdot 285 \cdot 10^3)^2 \cdot 467 \cdot 10^{-12}} = \frac{1}{1500} = 668 \mu\text{h}$
450	170	90	
570	94	64	
900	29	24	

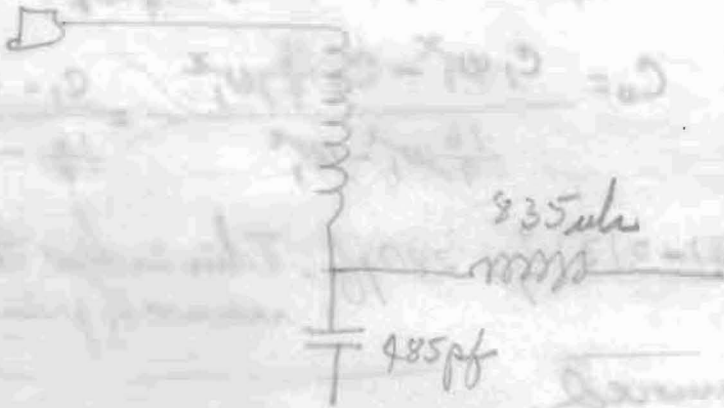
M B K Radio Repair Shop

(over)

Same but excess wire core removed

Freq	C	Q	$C_0 = \frac{450 - 4.99}{3} = \frac{54}{3} = 17 \mu\text{f}$
255	450	164	
350	230	109	$L_0 = \frac{1200}{(6.28 \cdot 255 \cdot 10^6)^2 \cdot 457 \cdot 10^{-12}} = 835 \mu\text{h}$
510	99	60	
800	29.3	24	

485 pf for resonance at 250 KC



HOBART, TASMANIA

(Proprietors: Australian National Hotels Ltd.)

West Point Riviera Hotel



TELEPHONE: 9516 (4 LINES) TELEGRAMS: "WEST POINT," HOBART

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Mixer Voltages & Currents

 $E_B = +142$, $E_C = +6$, $R_p = 100K\Omega$ $E_p + E_{sg} + E_g$
assumed from cathode

R_k	E_g	R_{sg}	E_{sg}	I_{sg}	E_p	I_p	Oscillator oscillation
15K	-1.3	290K	44V	.31ma	118V	.17ma	
10K	-1.6	170K	52V	.50ma	107V	.27ma	
10K	-2.6	125K	60V	.63ma	108V	.25ma	

use this condition

A mixer is needed which will pass more plate current for a given E_g , $E_{sg} + E_p$. Thus a lower screen voltage may be used and better ratio I_p/I_{sg} for a given E_g .

E_g must be 2V or more so that positive peaks (4.7V?) hit above by clipper will not allow grid to go to zero.

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Mixer Voltages. 1A7 Tube

220K Ω screen resistor $E_{SG} = 55V$ $I_{SG} = .51ma$

15K Ω cathode resistor $E_P = 159V$ $I_P = .13ma$

Bias +6V $E_K = +9.1V$ $I_K = .64ma$

220K Ω screen resistor $E_{SG} = 51V$ $I_{SG} = .53ma$

10K Ω cathode resistor $E_P = 159V$ $I_P = .29ma$

Bias +6V $E_K = +7.8V$ $I_K = .81ma$
changed osc anode grid #6 terminal to ground. No difference

Voltages on R.F tube 1LNS

15K Ω cathode resistor $E_P = 160V$ $I_P = 0.72ma$

Bias +6V $E_{SG} = 160V$ $I_{SG} = total$

$E_K = +10.2$ $I_K = .72ma$

~~15K 100K
 $E_P 160$ $E_{SG} 81$
 $I_P .04ma$ $I_{SG} .79ma$
 $E_K = 10.9V$
 $4\frac{1}{2}$
 10K 220K
 $E_P 160$ $E_{SG} 50V$
 $I_P .15ma$ $I_{SG} .87ma$
 $E_K = 14.7V$
 7.0~~

~~Mixer. ω collating Dial at 3000
 10K = R_K 100K = R_{SG}
 $E_P 160V$ $E_{SG} 72V$
 $E_K = 9.8V$ $I_P .15ma$ $I_{SG} .87ma$
 osc
 $R_K = 15K$ $R_{SG} = 220K$
 $E_P = 160V$ $E_{SG} = 57V$
 $E_K = 8.4V$ $I_P = .09ma$ $I_{SG} = .90ma$~~

Oscillator 30K Grid 100K plate

Dial	E_P	I_P	I_G	E_G	δ
0	43V	.74ma	.077ma	.115	7.7
45	43V	.76ma	.077ma	.102	7.0
100	46V	.71ma	.055ma	.073	5.2

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Oscillator Performance

$E_B = 162V$

$E_F = 1.57V$

1LN5 tube

Plate resistor 1.1 megohms, Grid resistor 0.23 megohms.

Dial	I_P	E_P	I_G	E_G
0	120 μ a	30V	35 μ a	8.1V
45	130 μ a	19V	40 μ a	9.2V
100	135 μ a	14V	4 μ a	9.4V

1A7-GT

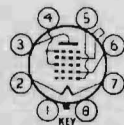
RADIOTRON

1A7-GT

PENTAGRID CONVERTER

Filament	Coated	
Voltage	1.4	d-c volts
Current	0.05	amp.
Direct Interelectrode Capacitances ⁰		
Grid #4 to Plate	0.5	μF.
Grid #4 to Grid #2	0.4	μF.
Grid #4 to Grid #1	0.2	μF.
Grid #4 to Grid #2	0.9	μF.
Grid #2 to All Other Electrodes (R-F Input)	7.0	μF.
Grid #2 to All Other Electrodes Except Grid #1 (Osc. Output)	4.4	μF.
Grid #1 to All Other Electrodes Except Grid #2 (Osc. Input)	3.4	μF.
Plate to All Other Electrodes (Mixer Output)	10.0	μF.
Maximum Overall Length	3-5/16"	
Maximum Seated Height	2-3/4"	
Maximum Diameter	1-5/16"	
Bulb	T-9	
Cap	Skirted Min.	
Base	Intermediate Shell Octal 8-Pin.	

Basing Designation	GT-7Z
Pin 1 - No	Pin 5-Grid #1
Pin 2-Filament	Pin 6-Grid #2
Pin 3-Plate	Pin 7-Fil.
Pin 4-Grids #3 & #5	Pin 8-No Con.
	Cap - Grid #4



Mounting Position Any

BOTTOM VIEW (GT-7Z)
Maximum Ratings are Design-Centre Values.
CONVERTER SERVICE

Plate Voltage	110 max. volts
Screen (Grids #3 & #5) Voltage	80 max. volts
Screen Supply Voltage	110 max. volts
Anode-Grid (Grid #2) Voltage	110 max. volts
Total Zero-Signal Cathode Current.	4 max. mA.

Typical Operation:	
Plate	90 volts
Screen **	45 volts
Anode-Grid	90 volts
Control-Grid (Grid #4)▲	0 volts
Oscillator-Grid (Grid #1) Resistor	200000 ohms
Plate Resistance	0.8 megohm
Conversion Transconductance	250 μmhos
Convers. Transcond. grid #4 bias of -3v.	5 approx. μmhos
Plate Current	0.6 mA.
Screen Current	0.7 mA.
Anode-Grid Current	1.2 mA.
Oscillator-Grid Current	0.035 mA.
Total Cathode Current	2.5 mA.

NOTE: The transconductance of the oscillator portion (not oscillating) is 550 micromhos under the following conditions: plate volts, 90; screen volts, 45; cont.-grid volts, 0; anode-grid volts, 90; and oscillator-grid volts, 0.
⁰ With close-fitting shield conn. to negative fil. terminal.
 ** Obtained preferably by using a properly by-passed 45000- to 75000-ohm voltage dropping resistor in series with the 90-volt supply.
 ▲ A resistance of at least 1.0 megohm should be in the grid return to negative filament pin.
 ← Indicates a Change.

AMALGAMATED WIRELESS VALVE CO. PTY. LTD.
DECEMBER, 1944 SYDNEY, AUSTRALIA

1A7-GT

RADIOTRON

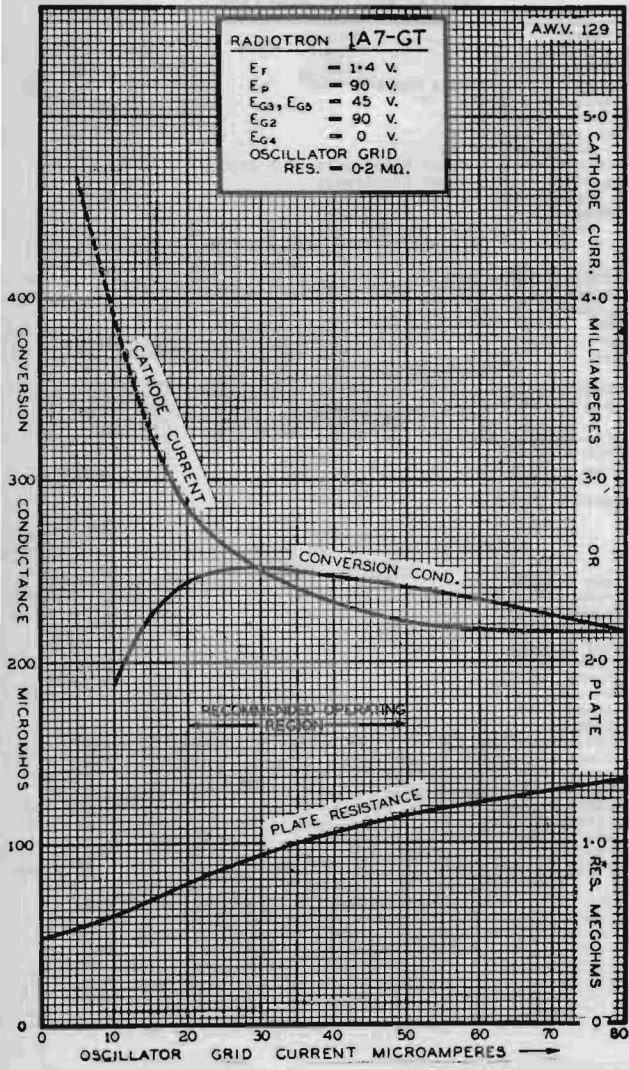
1A7-GT

OPERATION CHARACTERISTIC

RADIOTRON 1A7-GT

A.W.V. 129

- E_f = 1.4 V.
- E_p = 90 V.
- E_{G3}, E_{G5} = 45 V.
- E_{G2} = 90 V.
- E_{G4} = 0 V.
- OSCILLATOR GRID RES. = 0.2 MΩ.



$\frac{3}{4}$ " dia x 1" long
7 Pi coil with short core in center

Freq	Q	C
50	145	226.0
100	141	52.3
136.5	112	27.0

$$C_0 = \frac{226.0 - 4 \cdot 52.3}{3} = 5.6 \text{ pF}$$

$$L_0 = 43.9 \text{ mH}$$

Actual core is thus one part way
in one end.

1 June 57

Output R.F. coil for coupling between Maxon + 10,000 Ω pad. This coil same as one measured in 1954 on Maui. Made of 7/41 litz in 4 P_i with iron core. The two outside P_i wider than inside P_i . O.D. = 7/8"

Freq	Cap.	Q
60 KC	450 pf	111
90	196	132
120	107	135
180	45.4	115
227	27	91

$$C_0 = \frac{450 - 4 \cdot 107}{3} = \frac{450 - 428}{3} = \frac{22}{3}$$

$$= 7.3 \text{ pf}$$

$$L_0 = \frac{1}{(628 \cdot 06 \cdot 10^3)^2 \cdot 457 \cdot 10^{-12}} = \frac{1}{64.9}$$

$$= 15.4 \text{ mH.}$$

D.C. resistance 39 Ω

This is rebuilt coil of Feb 3, 1954

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Output Coil performance

In Air			Core Out			Core In		
Freq	Q	C	Freq	Q	C	Freq	Q	C
120 KC	103	450.0	120	104	426.0	90	115	427.5
240 KC	125	107.5	240	124	102.0	180	134	101.0
360 KC	102	46.5	360	100	43.6	240	119	54.0
459 KC	80	27.0	444	80	27.0	323	89	27.0

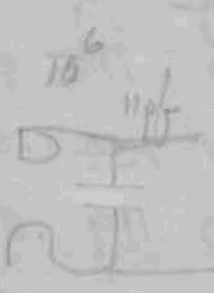
Obsolete on 1/6/57

This coil is center two P_n of coil
of 1/6/57

$$X_A = \frac{1}{6.28 \cdot 25 \cdot 10^6 \cdot 11 \cdot 10^{-12}} = \frac{10^4}{17.28} = 5800 \Omega$$

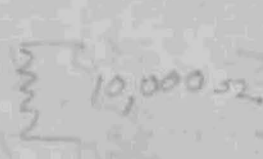
0 28.4 31.9 29.0
74.3 75.9 72.5 62.5

74.3 104.3 104.4 91.5



$$X_L = 2\pi fL$$

$$L = \frac{X_L}{2\pi f} = \frac{5800}{6.28 \cdot 25 \cdot 10^6}$$



$$= \frac{10^{-6}}{1.57} = \cancel{6.37} \times 10^{-7}$$

$$\begin{array}{r} 52.3 \\ 4 \\ \hline 209.2 \\ 226.0 \\ \hline 316.8 \\ 5.6 \end{array}$$

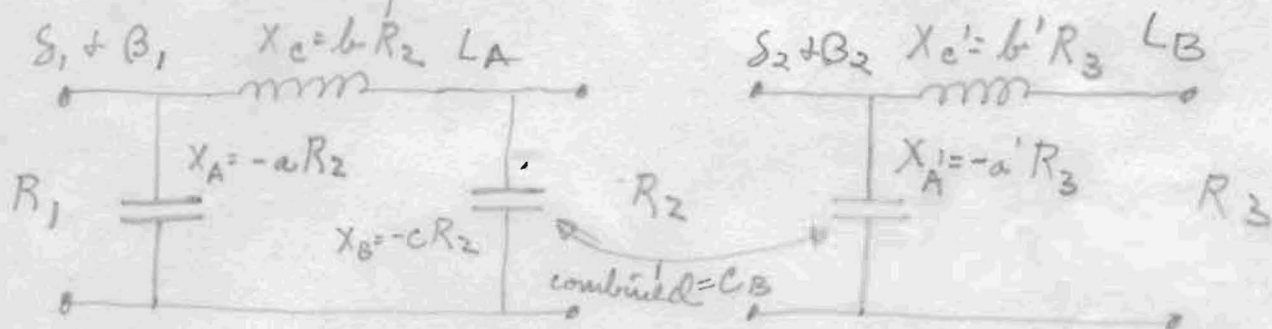
$$= \frac{X_L}{1.57} \times 10^{-6}$$

$$\begin{array}{r} 23 \\ 65.9 \\ 4 \\ \hline 263.6 \\ 275.5 \\ \hline 341.9 \\ 4.0 \mu\text{H} \end{array}$$

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Network between Mixer Plate + Filter

See Terman page 210-214 and figures 75-80



$R_1 = 10^6 \Omega$, $R_3 = 10^4 \Omega$ Frequency = 250 Kc, $C_A = 11 \text{ pf}$, $X_A = 58000 \Omega$

R_2 (by definition)	10000	15000	20,000	30,000
R_2/R_3	1	1.5	2.0	3.0
a' (from Fig 75, Locus for L section)	∞	2.25	2.0	2.2
$X_{A'}$, $X_{A'} = -a'R_3$	∞	-22500	-20000	-22000
b' (from Fig 76, Locus for L section)	0	.7	1.0	1.45
$X_{c'}$, $X_{c'} = b'R_3$	0	7000	10000	14500
β_2 (from Fig 76, Locus for L section)	0	-35°	-45°	-55°
δ_2 (from Fig 80, Locus for L section)	-	.8	1.0	1.4
R_1/R_2	100	67	50	33
a , $a = 58000/R_2$	5.8	3.9	2.9	1.93
β_1 (from fig 75, $\beta > 90^\circ$)	-141°	-147°	-152°	-157°
δ (from fig 79)	19	18	19	20
b (from fig 76)	6.0	4.3	3.2	2.7
X_c , $X_c = bR_2$	60,000	64000	64000	66000
c (from Fig 77)	.71	.56	.44	.34
X_B , $X_B = -cR_2$	-7100	-8400	-8800	-10200
L_A	38.2 mH	40.8	40.8	42.1
L_B	0	4.46 mH	6.36	9.25
C_B	74.3 pf	104.3	104.3	91.5

1/6/57

Filter Design Continued.

	V _{out} - over				
R ₂	40,000	50,000	60,000	70,000	80,000
R ₂ /R ₃	4.0	5.0	6.0	7.0	8.0
a ₁	2.3	2.5	2.65	2.8	3.0
X _{a1}	-23000	-25000	-26500	-28000	-30000
b ₁	1.75	2.0	2.2	2.4	2.6
X _{e1}	17500	20000	22000	24000	26000
β ₂	-60°	-65°	-69°	-70	-72°
δ ₂	1.7	2.0	2.2	2.4	2.55
R ₁ /R ₂	25	20	16.7	14.3	12.5
a	1.45	1.16	.97	.833	.725
β ₁	-160°	-162°	163°	163°	163°
δ	21	21	22	21	20
b	1.7	1.4	1.2	1.05	.92
X _e	65,000	70,000	72,000	73,000	74,000
c	.295	.26	.235	.22	.21
X _B	-11,800	-13000	-14000	-15000	-16800
L _A	43.4	44.5	45.9	46.5	47.1
L _B	11.1	12.8	14.0	15.3	16.6
C _B	82.0	74.7	69.6	64.3	59.3