

27/9/66

RF Tuner Performance

Source 50 ohms

Output across secondary of double tuned circuit

Low End				Middle				High End			
KC	Input mV	Output Volts	DB	KC	Input mV	Output Volts	DB	KC	Input mV	Output Volts	DB
1500	200	.02		1700	200	.03		1800	200	.03	
1600	200	.080		1900	100	.095		1900	200	.05	
1700	50	.055		2000	50	.190		2000	200	.09	
1800	20	.265		2060	20	.375		2100	100	.10	
1850	10	.320		2100	10	.64		2200	50	.135	
1860	5	.715		2120	5	.72		2300	20	.42	
1870	5	.870		2130	5	.895		2350	10	.78	
1887	5	.815		2140	5	.965		2370	5	.785	
1903	5	.855		2148	5	.960		2380	4	.82	
1915	5	.710		2158	5	.970		2400	4	.88	
1930	10	.670		2170	5	.905		2420	4	.745	
2000	20	.12		2180	5	.660		2430	5	.70	
2100	200	.12		2200	10	.535		2450	10	.605	
2200	200	.03		2250	20	.24		2500	20	.285	
				2300	100	.24		2550	50	.165	
				2400	200	.12		2600	100	.155	
				2500	200	.03		2700	200	.100	
								2800	200	.050	
								2900	200	.02	

27/9/66

Input Circuit Performance

Source 50 ohms. Primary 5 turns
 Secondary
 Tertiary 3 turns

viral over secondary

lit_y over secondary.

No Current in Transistor				Transistor Current 2ma Collector Grounded				Output Circuit operative			
KC	Input mV	Output volts	DB	KC	Input mV	Output volts	DB	KC	Input mV	Output volts	DB
500	200	.03		200	.12			200	.03		
1000	200	.12		200	.125			200	.125		
1500	100	.12		100	.125			100	.12		
1700	50	.145		50	.12			50	.115		
1800	20	.135		20	.08			20	.06		
1865	20	.235		20	.10			1865	20	.135	
1950	20	.12		20	.09			1895	20	.105	
2100	50	.12		50	.11			1920	20	.135	
2400	100	.11		100	.10			1950	20	.095	
3000	200	.115		200	.115			2100	50	.105	
5000	200	.04		200	.04			2400	100	.100	
								3000	200	.115	
								5000	200	.04	

Transistor input Circuit

26/9/66

Input 183 mw to primary.

Output across tuned secondary.

		KC	Volts		
Unloaded.	3DB	1859	.28	9KC	19KC wide.
	Peak	1868	.40	10KC	
	3DB	1878	.28		
Current in transistor but collector shorted.	3DB	1850	.14	18KC	38KC wide
	Peak	1868	.20	20KC	
	3DB	1888	.14		
Collector in circuit	3DB	1860	.27	8KC	17KC wide
	Peak	1868	.38	9KC	
	3DB	1877	.27		

Output across secondary of double tuned pair.
Input 17.8 mw.

Edge	1855	.54	12KC	
Peak	1867	1.00	25KC	
Dip	1892	.54	18KC	43KC wide.
Peak	1910	.98	5KC	
Edge.	1915	.54		

Emitter winding $1\frac{1}{4}$ turns over secondary.

Primary 7 turns $\frac{5}{8}$ " dia and $\frac{5}{8}$ " from bottom end secondary.

System obviously has feedback and needs to be neutralized.

Small mutual and still less top capacity ^{1.8 pf approx} Range 511 KC

Peak	1856	.90	2066	.83	2360	.79
Dip	1888	.50	2100	.53	2399	.57
Peak	1921	.96	2139	.87	2430	.74
Width	65		73		70	
Avg. Max		.93		.85		.77
DB Dip	5.4		4.1		2.6	

Decreased mutual & about 1.8 pf top Range 514 KC

Peak	1861	.92	2077	.84	2368	.84
Dip	1882	.63	2100	.67	2396	.72
Peak	1912	1.00	2125	.91	2418	.78
Width	51		48		50	
Avg. Max		.96		.90		.81
DB Dip	3.6		2.6		1.0	

10mv input. Output 5 turns over sec to base of grounded emitter mixer. Decided to leave in this condition.

Range should be reduced to 450 KC by removing turn from coils

Capacity ratio = $\left(\frac{2396}{1882}\right)^2 = 1.620 \text{ to } 1$ Minimum = $\frac{1000}{.620} \cdot 102 = 165 \text{ pf}$

$L = 1 / (6.28 \cdot 1.882)^2 (165 + 102) = 1 / 139,8 \cdot 267 = 10^{-6} / .0573$

= 26.8uh effective in coil at $21\frac{1}{2}$ turns.

Desired = 23.9uh

Required turns = $\left(\frac{23.9}{26.8}\right)^{1/2} 21.5 = 20.3 \text{ turns}$

Required to remove one turn from coils.

Spacing between bottom edges of coil supports $10\frac{1}{2} / 32 = 21/64$ "

- 145 shunts
- 11 gages
- 3 coils
- 6 transistor
- 165 total

23/9/66

23/9/66

Double Tuned Circuit + Compound Coupling

Coils $21\frac{1}{2}$ turns $75/\#44$ Litz. Input 10mv, Output = volts.

Transistor grounded base, collector at top of primary.
Each transistor draws 2ma at 7volts, 500 Ω emitter resistor.

Low Frequency

Medium Frequency

High Frequency

KC Output

KC Output

KC Output

Small mutual and top capacity

Range 480 KC

Peak	1851	.96	2083	.93	2340	3DB
Dip	1872	.69	2100	.82	2352	101
Peak	1894	.96	2118	.89	2376	3DB
Width	43		35		36	
Avg. Max		.96		.91		
DB dip	2.9		0.9		12	

Larger mutual and same top capacity

Range 486 KC

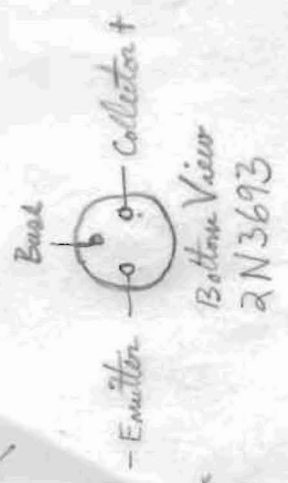
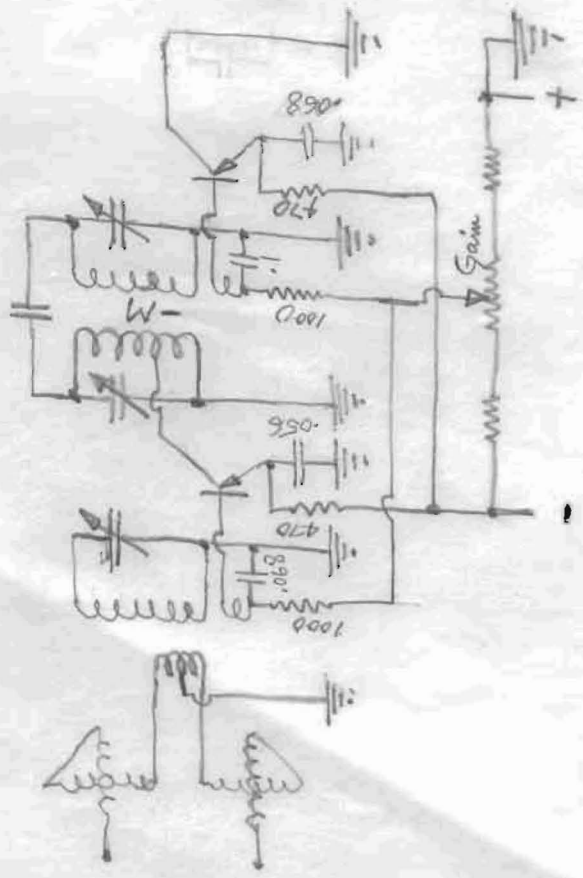
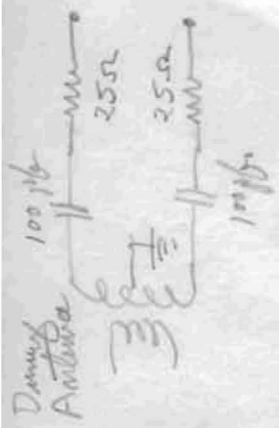
Peak	1831	.92	2058	.85	2325	.82
Dip	1875	.43	2093	.49	2361	.56
Peak	1912	.94	2138	.86	2399	.73
Width	81		80		74	
Avg. Max		.93		.855		.775
DB dip	6.7		4.8		2.8	

Small mutual and better top capacity

Range 509 KC

Peak	1858	.88	2076	.80	2364	.78
Dip	1881	.56	2103	.60	2390	.69
Peak	1916	.99	2132	.91	2412	.80
Width	58		56		48	
Avg. Max		.94		.86		.79
DB dip	4.5		3.1		1.2	

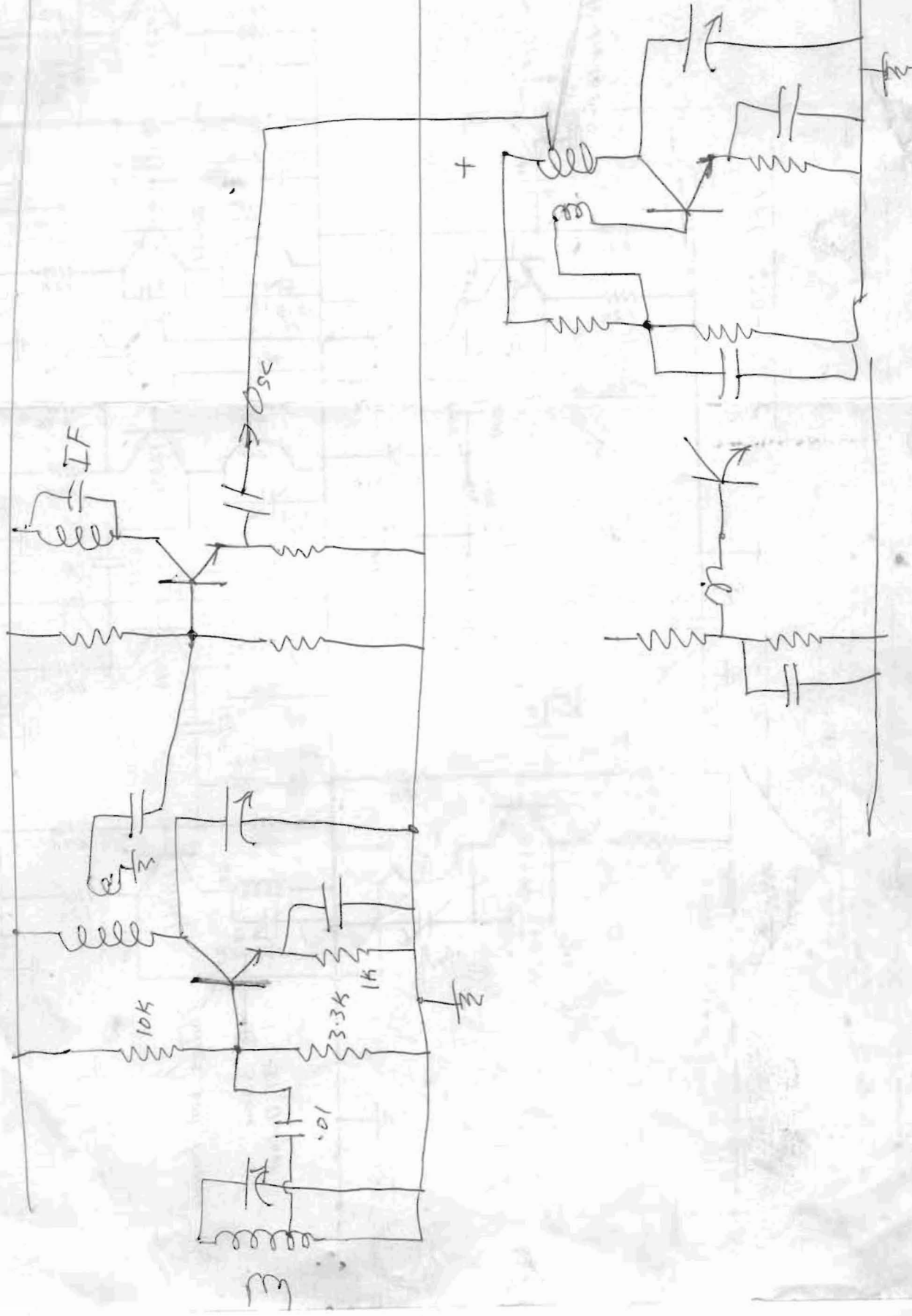
20/9/66



$$24 \mu\text{h} = \left(\frac{24}{32.7} \right)^{1/2} 25T = 21.9 \text{ turns}$$

Eddystone Radio Ltd
Birmingham 31, England

→ Eddystone model EC
sold by R. H. Curwin



MC

Q R

2/9/66

1.5 387 278
 2.1 198 269
 3.0 95 235
 4.2 47 188

42 T, 125/#44 Litz, close wound
 37.5mm long, 29.6mm dia
 9.85mm dia
 In Air

$C_0 = 2.7 \text{ pf}$
 $L = 28.9 \text{ } \mu\text{h}$

Same wire as 47T 26.2mm dia

5/9/66

1.5 356 419
 2.1 182 370
 3.0 87.5 296
 4.2 44 228
 1.5 390 371
 2.1 200 340
 3.0 95.5 282
 4.2 47.5 221

25 T, 125/#44 Litz, close wound, 0.85mm dia
 21.2mm long, 16.7mm dia
 With core in can
 $\frac{1}{2}$ " dia x $1\frac{1}{2}$ "

$C_0 = 2.0 \text{ pf}$
 $L = 31.5 \text{ } \mu\text{h}$
 $R =$

In copper can

2 7/8" dia x 4" long

 $C_0 = 3.0 \text{ pf}$ $L = 28.7 \text{ } \mu\text{h} = -8.9\%$ $R =$

Q at 2.1mc - 8.0%

1.5 315 480
 2.1 160 434
 3.0 77 340
 4.2 38.2 258

25 T, 75/#44 Litz, close wound, 1.70mm dia
 17.5mm long, 16.4mm dia
 With core in air
 $\frac{1}{2}$ " dia x $1\frac{1}{2}$ "

$C_0 = 2.3 \text{ pf}$
 $L = 35.6 \text{ } \mu\text{h}$

In copper can

2 7/8" dia x 4" long

 $R =$ $C_0 = 4.3 \text{ pf}$ $L = 32.7 \text{ } \mu\text{h} = -8.2\%$ $R =$

Q at 2.1mc - 13.3%

1.5 340 467
 2.1 173 376
 3.0 82 304
 4.2 39.7 222

Think this coil had
 some broken strands
 in the Litz when
 in the can

Coil tests in $2\frac{1}{2} \times 2\frac{1}{2} \times 3\frac{1}{2}$ Cans Aluminum 2/9/66

MC pf Q R all coils air core. PMG, Q machine

57T, .22mm wire, 25.4mm long, 16.1mm dia.

1.5 442 74

2.1 226 88

3.0 109 104

4.2 54 118

1.5 437 77

2.1 224 92

3.0 108 110

4.2 54 128

In Can $C_0 = 2.7 \text{ pf}$

$L = 25.3 \mu\text{h} = -1.6\%$

R =

2.1mc Q = -4.4%

In Air $C_0 = 2.1 \text{ pf}$

$L = 25.7 \mu\text{h}$

R =

48T, .39mm wire, 37.3mm long, 22.6mm dia.

1.5 490 84

2.1 250 99

3.0 120 115

4.2 60 128

1.5 468 108

2.1 240 128

3.0 115 152

4.2 58 175

In Can $C_0 = 3.3 \text{ pf}$

$L = 22.8 \mu\text{h} = -4.6\%$

R =

2.1mc Q = -22.6%

In Air $C_0 = 2.7 \text{ pf}$

$L = 23.9 \mu\text{h}$

R =

2/9/66

MC Pf Q R

46T, .54mm wire, 49.2mm long, 29.1mm dia

1.5 445 82

In Can $C_0 = 4.7 \mu\text{f}$

2.1 227 95

$L = 25.1 \mu\text{h} = -9.3\%$

3.0 108 110

R =

4.2 53 120

2.1 mc Q = -44.1%

1.5 405 145

In Air $C_0 = 1.7 \mu\text{f}$

2.1 205 170

$L = 27.7 \mu\text{h}$

3.0 100 205

R =

4.2 50 231

4 1/2 T, Litz, close wound
29.0mm long, 26mm dia
Wire 0.70mm dia

25 μh standard inductor.

Can
struc.

Can 2 1/2" dia, 3 1/4" long. copper.

1.5 454 255 .909 .005

In Can $C_0 = 4.8 \mu\text{f}$

2.1 231 288 1.126 .014

$L = 24.6 \mu\text{h} = -3.7\%$

3.0 110 294 1.576 .041

$R = 154.5 \frac{\text{MC}}{\text{Q}}$

4.2 54 263 2.469 .100

Q = -7.2% at 2.1mc.

1.5 415 279 .904

In Air $C_0 = 5.3 \mu\text{f}$

2.1 212 310 1.140

$L = 26.8 \mu\text{h}$

3.0 101 312 1.617

$R = 168.2 \frac{\text{MC}}{\text{Q}}$

4.2 49 275 2.569

Litz many very fine strands. Probably greater than 75 strands and finer than #44

MC pf Q R

2/9/66

36T, 21-#41B+S Litz, 32 mm long, 29 mm dia
In Can Co = 0.49 mm O.D.

1.5
 2.1
 3.0
 4.2

1.5	465	146
2.1	238	163
3.0	115	167
4.2	57	161

L=
R=

In Air Co = 2.5 pf
L = 24.1 μ h
R =

50T, 200-#99 Litz, 42 mm long
1.05 mm dia, 30 mm dia
14 turns in bamps at center,
In Can

1.5 284 263
 2.1 175 210
 3.0 68 156
 4.2 116

In Air Co = 4.0 pf
L = 39.1 μ h

Had 42T for 27.5 μ h.

MC pf Q R

2/9/66

47T, 125/#44 litz, close wound, .85mm dia
40.5mm long, 26.2mm dia. dia

1.5 390 292

In air $C_0 = 2.3\%$
 $L = 28.7 \mu H$

2.1 200 261

3.0 96 226

4.2 48 181

1.5

In $2\frac{1}{2}$ dia x $3\frac{1}{4}$ " copper can

$C_0 =$

2.1 223 235

$L = -10.2\%$

3.0

$Q = -10.0\%$ at 2.1mc

4.2

43T, 75/#44 Litz, close wound, .70mm dia
29.7mm long, 26.1mm dia.

1.5 375 272

In air $C_0 = 2.3\%$

2.1 191 274

$L = 29.9 \mu H$

3.0 92 249

4.2 46 210

In $2\frac{1}{2}$ dia x $3\frac{1}{4}$ " copper can

2.1 213 248

$L = -10.2\%$

$Q = -9.4\%$ at 2.1mc

This Litz not quite as good as in standard inductor

PMG machine

28 turns, .46 mm wire spaced wound, $5/8''$ dia x $1''$ long ^{1/9/66}

MC	pf	Q	R	skull diam.
1.5	341	95	2.25	.54
2.1	173	109	3.97	1.86
3.0	83	121	5.10	2.34
4.2	41	128	6.76	2.97
1.5	-?	70	.84	.03
2.1	920	84	.98	.00
3.0	449	102	1.16	.05
4.2	229	121	1.36	.05

In can $2\frac{1}{2} \times 2\frac{1}{2} \times 3\frac{1}{2}$ al.

With coil

$$C_0 = 3.0$$

$$L = 32.8 \mu\text{h}, = -10.4\%$$

$$R = 20.6 \frac{\text{MC}}{\text{Q}}$$

$$\mu = 5.24$$

Less coil

$$C_0 = 1.3 \text{ pf}$$

$$L = 6.26 \mu\text{h} -1.8\%$$

$$R = 39.3 \frac{\text{MC}}{\text{Q}}$$

MC	pf	Q	R	skull diam.	Coil diam.
1.5	305	202	1.71	.90	
2.1	154	229	2.11	1.13	
3.0	74	250	2.76	1.65	
4.2	37	255	3.79	2.48	
1.5	-?	74	.81		wire diam.
2.1	904	86	.98		
3.0	440	108	1.11		
4.2	225	129	1.31		

In air

With coil

$$C_0 = 3.0$$

$$L = 36.6 \mu\text{h}, \mu = 5.74$$

$$R = 230 \frac{\text{MC}}{\text{Q}}$$

Less coil

$$C_0 = 1.3 \text{ pf}$$

$$L = 6.38 \mu\text{h}$$

$$R = 40.1 \frac{\text{MC}}{\text{Q}}$$

$$26.3 \mu\text{h} = 23.6 \text{ T}$$

$$\begin{matrix} 730 & 130 & 53 \\ 124 & 732 & 10 \\ 904 & 720 & 47 \end{matrix}$$

PMG machine

26T, .98mm wire close wound,

1/9/66
 5/8" dia x 1" long
I mean

ME	ρ	Q	R	shield class.	Notes
1.5	415	53	4.8	.7	Wire Core. $C_0 = 3.7 \mu F$
2.1	213	59	6.0	.9	$L = 26.9 \mu H$ -10.6% $\mu = 5.07$
3.0	101	65	7.8	1.2	$R = 169 \frac{MC}{Q}$
1.5	2140	69	.72	.05	Less Core
2.1	1090	81	.86	.05	$C_0 = 2.0 \mu F$
3.0	529	95	1.05	.08	$L = 5.30 \mu H$ -1.4%
4.2	271	111	1.26		$R = 33.3 \frac{MC}{Q}$

ME	ρ	Q	R	shield class.	Notes
1.5	371	69	4.1	3.3	Core in Air wire core $C_0 = 2.7 \mu F$
2.1	190	78	5.1	4.3	$L = 30.1 \mu H$ $\mu = 5.60$
3.0	91	86	6.6	5.6	$R = 189 \frac{MC}{Q}$
1.5	2110	65	.77		Less core $C_0 = .3 \mu F$
2.1	1077	87	.81		$L = 5.37 \mu H$
3.0	524	104	.97		$R = 33.7 \frac{MC}{Q}$
4.2	269	122			

26.3 μH =
 24.3 T
 358 240 375
 738 730 210
 1090 110
 210

2/9/66

Tuning rate = 5 KC per division = 500 cps per 0.1 division.
allow 50 KC contraction at ends of range.

Net range 450 KC = 1900 - 2350 KC

Tuning range = $\frac{2350}{1900} = 1.237$

Capacity range = $1.237^2 = 1.530$

Capacity variation = 102 pf.

Minimum capacity = $\frac{102}{1.530} = 66.7$ pf.

$L = \frac{1}{(6.28 \cdot 1.9)^2} 294.5 = \frac{1}{142.2} \cdot 294.5 \cdot 10^{-6} = 2.07 \mu\text{h}$

allow 10% for reduction in can = 26.3 μh in air

30/8/66

4 gang Condenser, Front to Back

Gang	Max	Min	Range
1	111.0	8.0	103 pf
2	111.0	8.0	103 pf
3	110.0	8.0	102 pf
4	113.0	11.0	102 pf

PMG machine

1/9/66

Variometer

MC pf Q R

.75 245 94 8.5

1.05 114 82 13.7

1.5 46 56 28.6

.75 -? 31 2.9

1.05 1190 37 3.4

1.5 575 44 4.0

2.1 285 48 5.2

3.0 127 48 7.4

4.2 53 39 12.8

Max inductance

$C_0 = 20.3 \text{ pf}$

$L = 170 \mu\text{h}$

$R = 1067 \text{ Mc/Q}$

Min inductance

$C_0 = 23.3 \text{ pf}$

$L = 18.8 \mu\text{h}$

$R = 118 \text{ Mc/Q}$



RAYTHEON COMPANY

SEMICONDUCTOR OPERATION

350 ELLIS STREET
MOUNTAIN VIEW, CALIFORNIA

AREA CODE 415
PHONE 968-9211
TWX 969-9190

July 19, 1965

Mr. Grote Reber
Tasmanian Regional
Laboratory, CSIRO
"Stowell", Stowell Avenue
Hobart, Tasmania
Australia

Dear Mr. Reber:

Reference is made to your inquiry of July 15, 1965. The specification sheets for the FN1024 and FN1034 Field Effect Transistors are indeed similar. The devices are selected to different specifications, however.

You will find the drain characteristics chart on page 3, top center of FN1024 quite accurate. This is a representation of typical characteristics and should be evaluated with this fact in mind.

The Raytheon FET has an insulated gate and the input resistance (R_g) does not change noticeably with a change in electrical parameters within the maximum ratings of the device. (This input resistance is the dielectric resistance of silicon dioxide). It is in excess of $10^{12} \Omega$ if the glass between the gate lead and all other leads is kept clean.

Very truly yours,

D. W. Hollenbeck

/dm

cc: E. Ziegler

15th July, 1965.

Raytheon Company,
Semiconductor Operation,
350 Ellis Street,
Mountain View,
CALIFORNIA...U.S.A.

Dear Sirs,

Recently I have secured product specification sheets issued 2-65 on your types FN1024 and FN1034 field effect transistors from your Mr. E. Ziegler of your New York office. The small charts showing drain current versus drain voltage for typical V_{GSB} at $+25^{\circ}C$ and $+125^{\circ}C$ are identical for both transistors. These charts are quite similar at $-200^{\circ}C$. Unfortunately the large chart covering page 4 of sheet for FN1024 is markedly different from small chart at top centre of page 3. Which one is correct?

On page 3 near bottom under Typical Values for FN1024, item 1 lists $R_G = 10^{15}$ ohms. The specified conditions of $V_{DSB} = -10$ volts and $I_D = -1.0$ ma are quite far from centre of dynamic working range. I suspect R_G decreases rapidly as V_{GSB} becomes more negative and I_D becomes larger. Please send to me curves of R_G versus V_{GSB} for typical values of V_{DS} . This information in some other form such as tables of values will be quite satisfactory.

Yours faithfully,

Grote Reber.

GR:JEG

RAYTHEON

RAYTHEON COMPANY

REGIONAL COMMERCIAL SALES

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ENGLEWOOD CLIFFS, NEW JERSEY 07632
AREA CODE 201-DIAL: 567-4911
MANHATTAN TELEPHONE:
AREA CODE 212-WISCONSIN 7-6400

June 30, 1965

Mr. Grote Reber
Research Corporation
405 Lexington Avenue
New York, N. Y. 10017

Dear Mr. Reber:

In accordance with your request, we are pleased to enclose data sheets FN1034 and FN1024 on our Field Effect Transistors.

Thank you for your interest in Raytheon products and, if we can be of further assistance, please feel free to contact the writer.

Yours very truly,

RAYTHEON COMPANY

E. Ziegler
E. Ziegler
District Sales Engineer
Components Division

Enclosures