

The Genesis of SIS Mixers – The Legacy of John Tucker in Radio Astronomy

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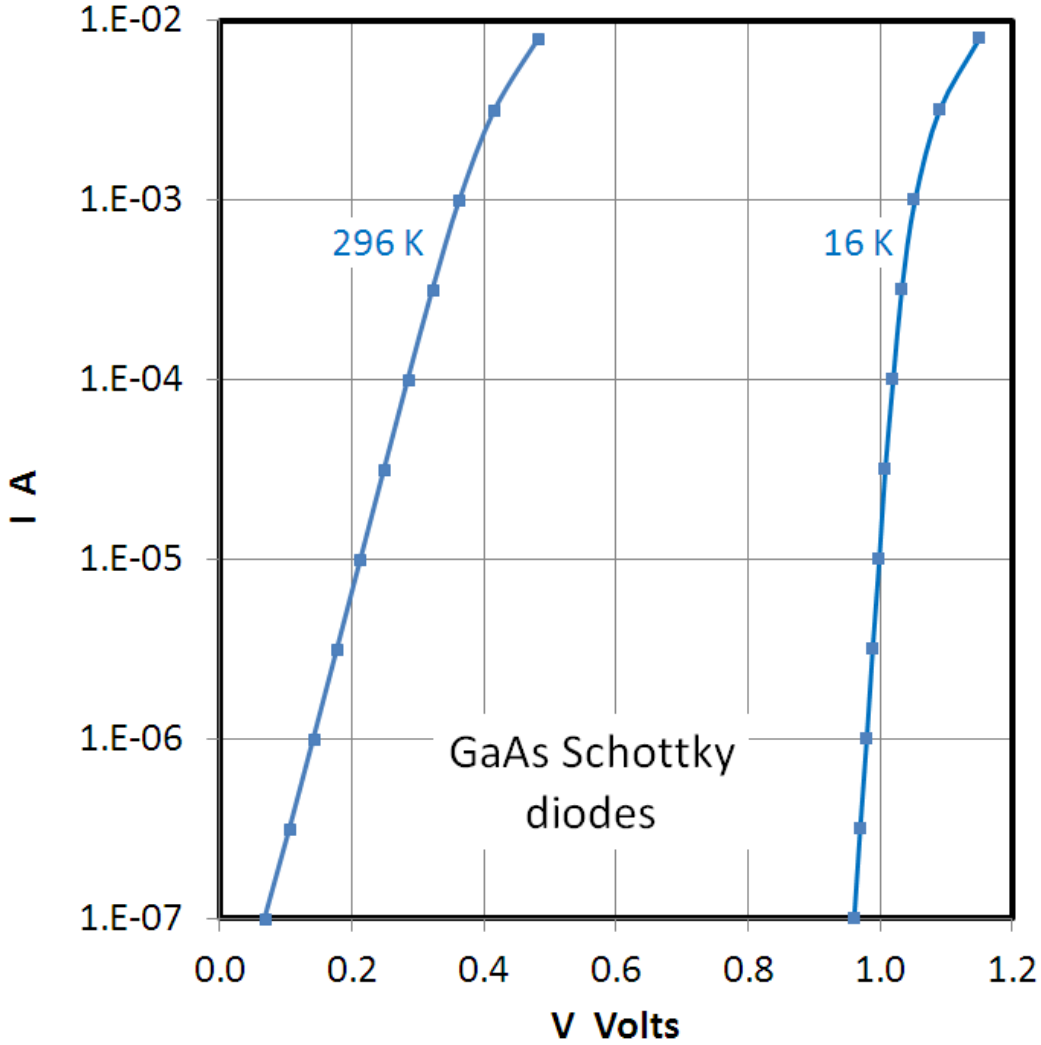


WE3E-1

IMS 2015
Phoenix



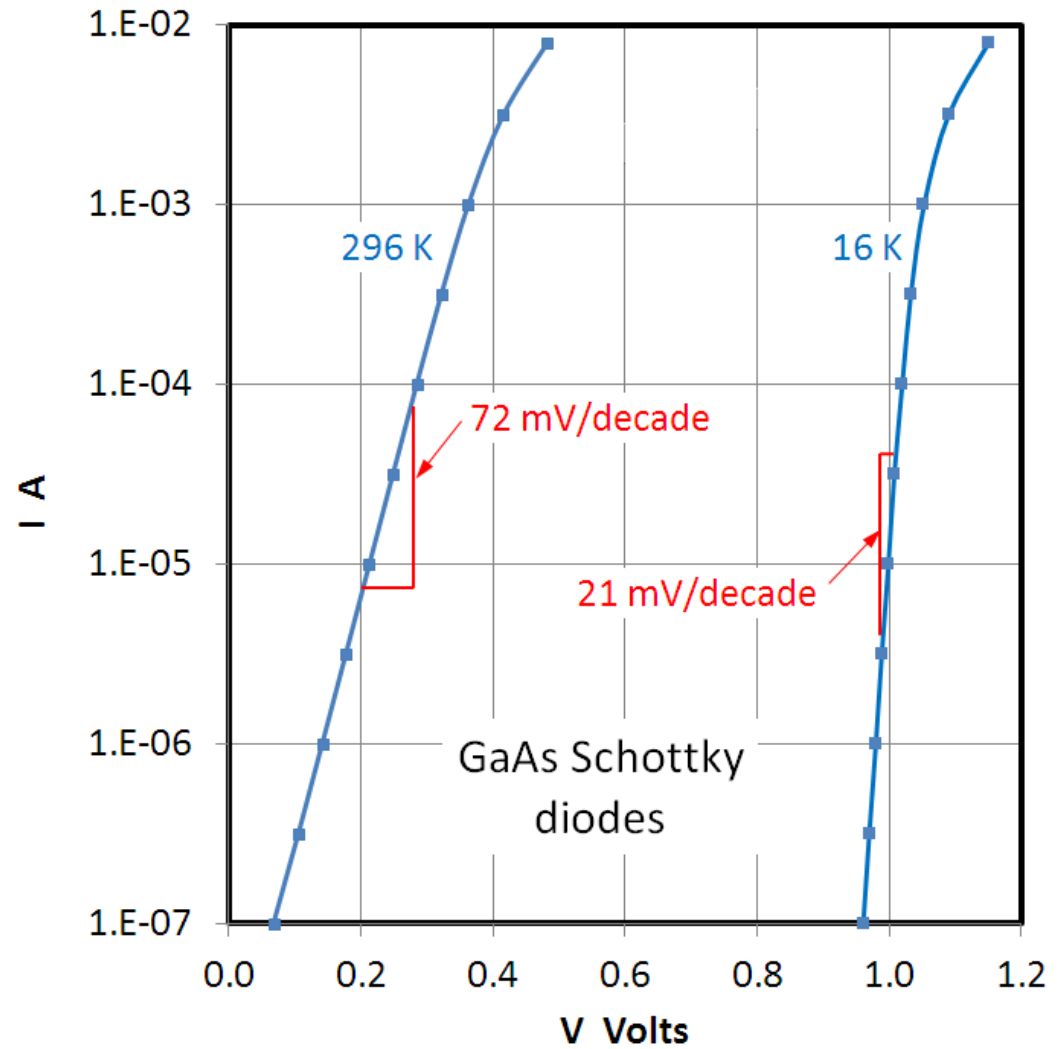
Schottky diode



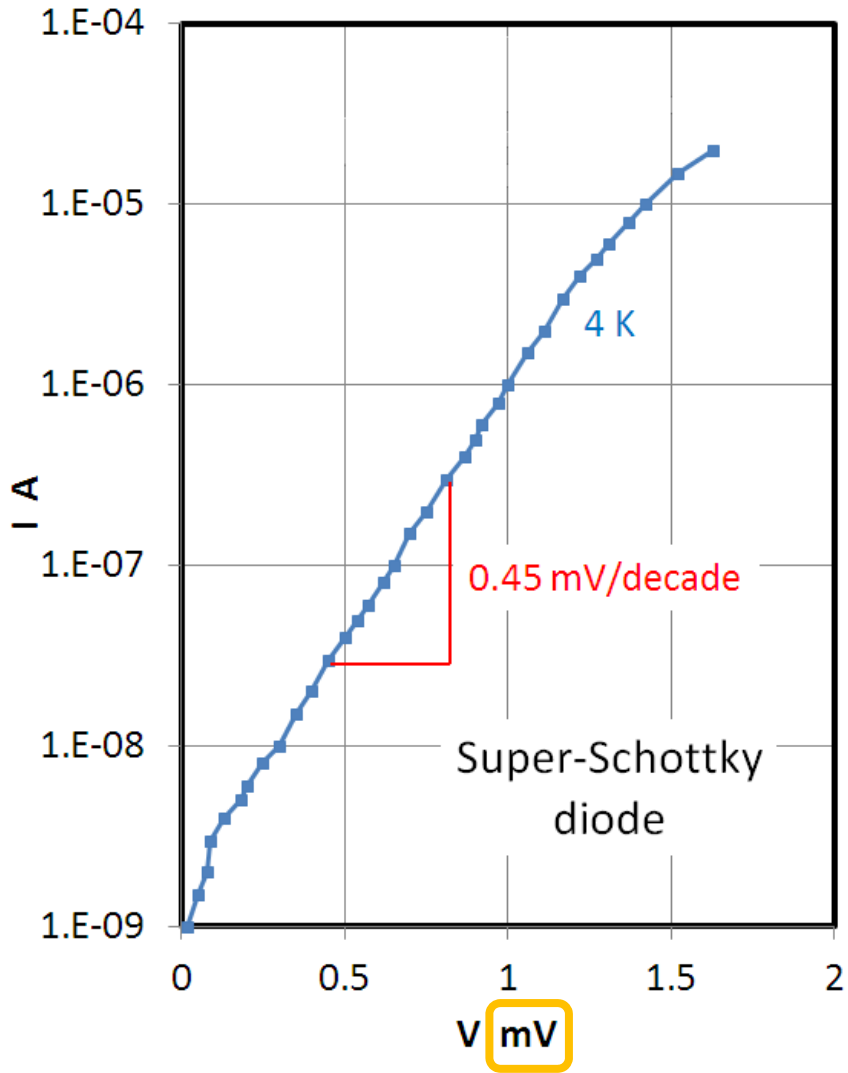
Schottky diode

For an exponential diode
the incremental conductance:

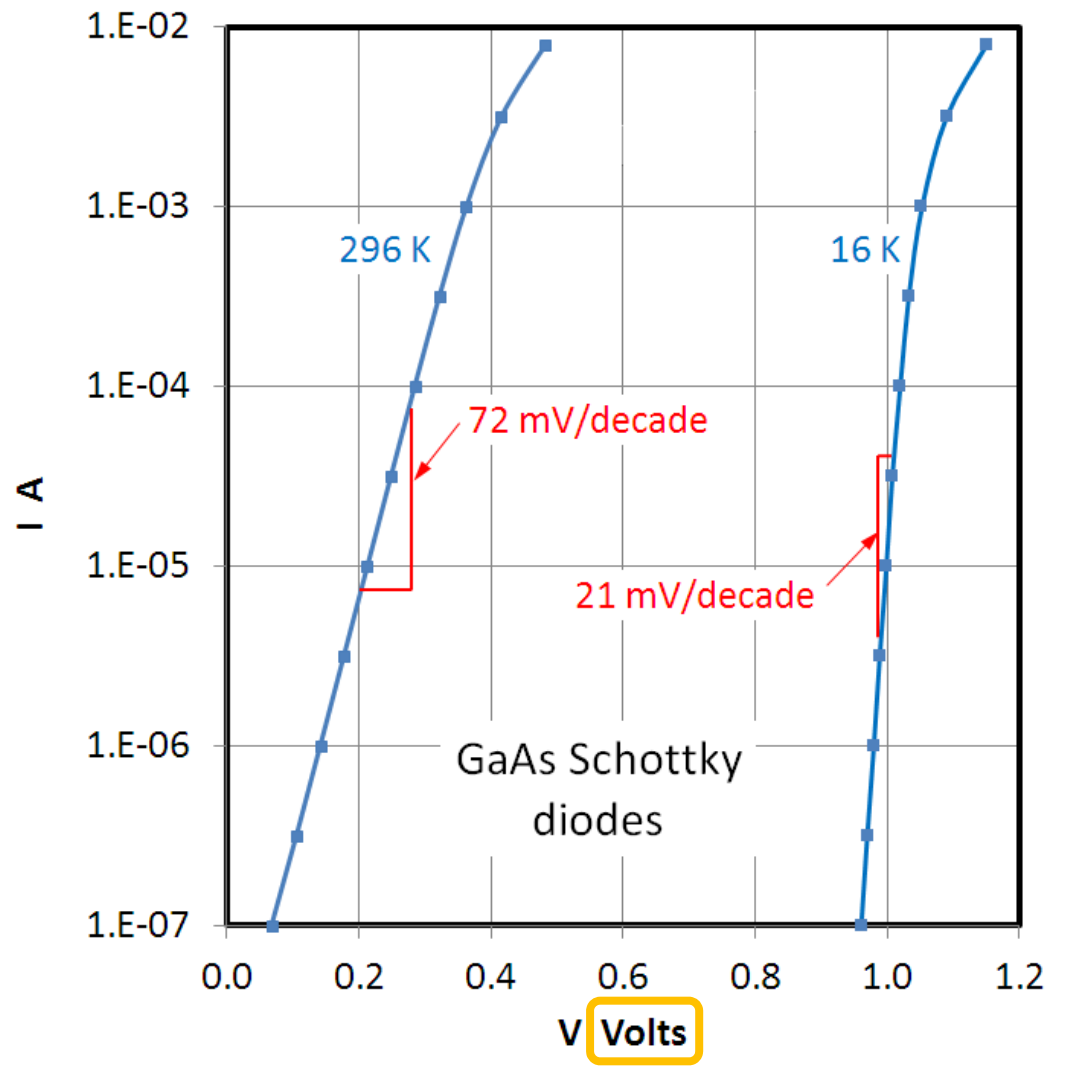
$$\frac{di}{dv} \approx \left[\frac{e}{\eta kT} \right] i$$



Super-Schottky diode

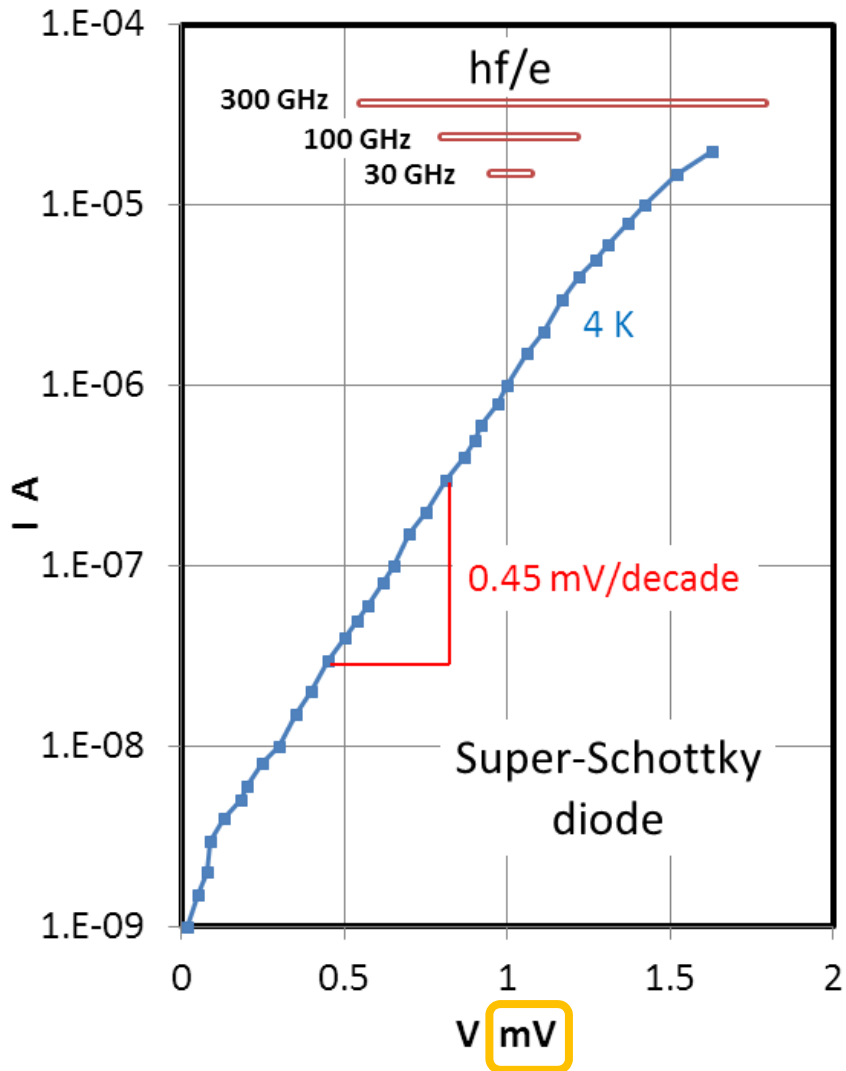


Schottky diode

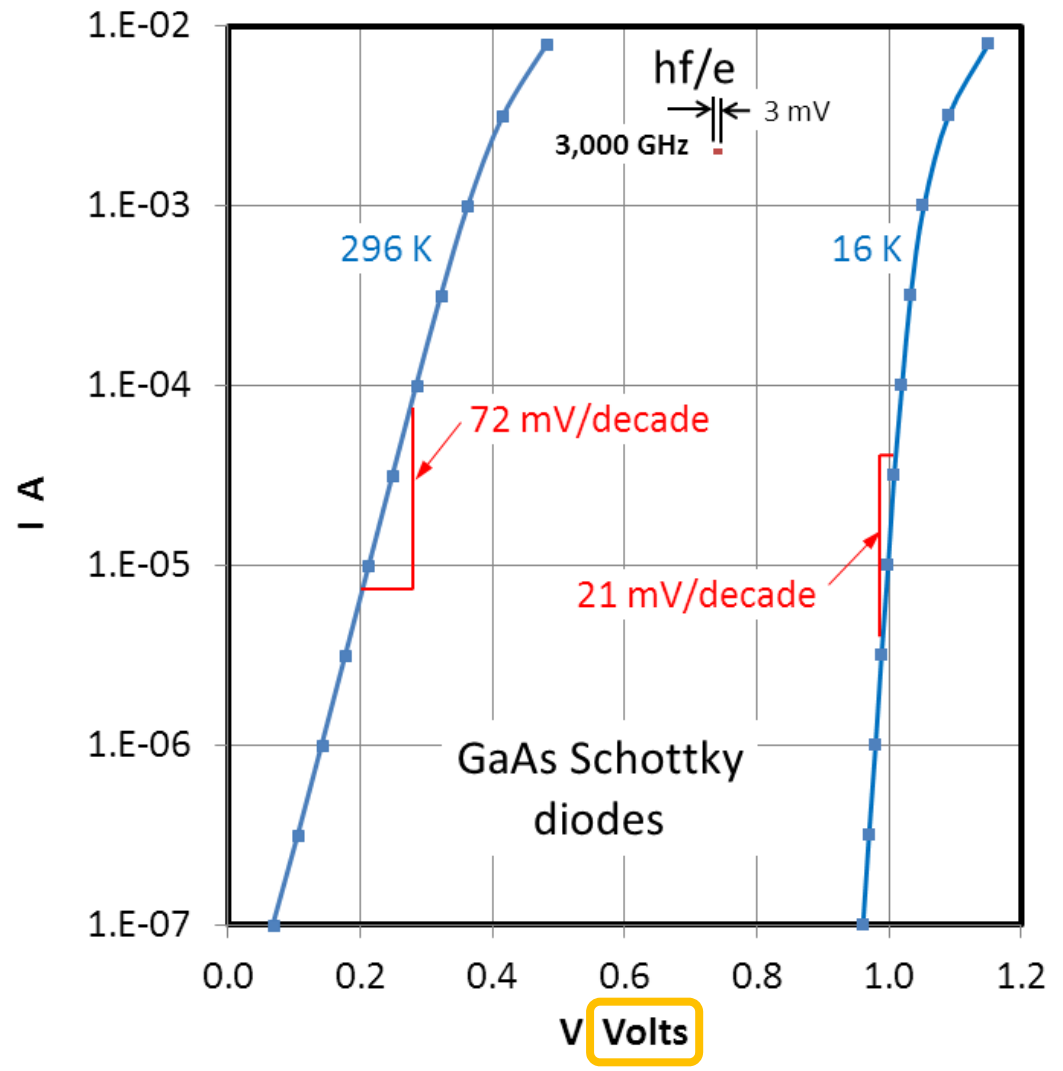


Quantum mixing effects become significant when the diode conductance changes significantly on the scale of the photon voltage hf/e .

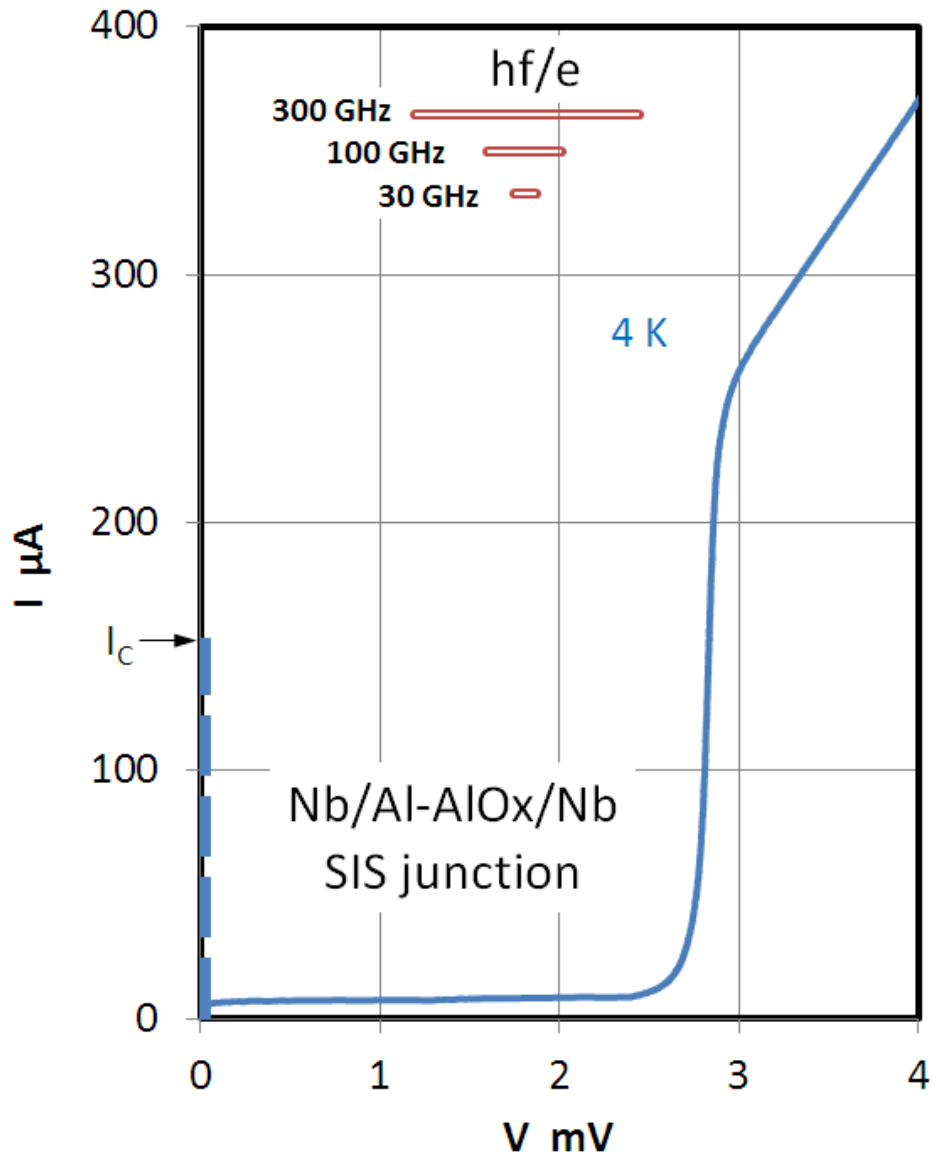
Super-Schottky diode



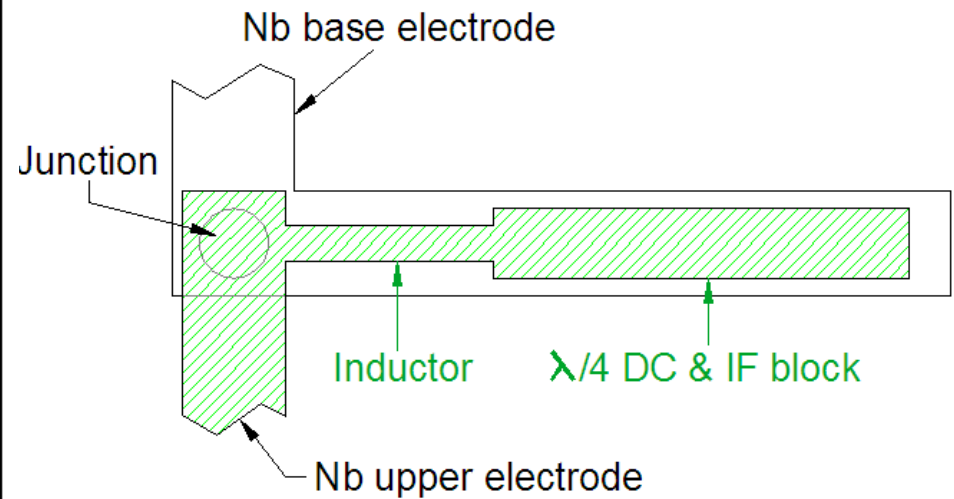
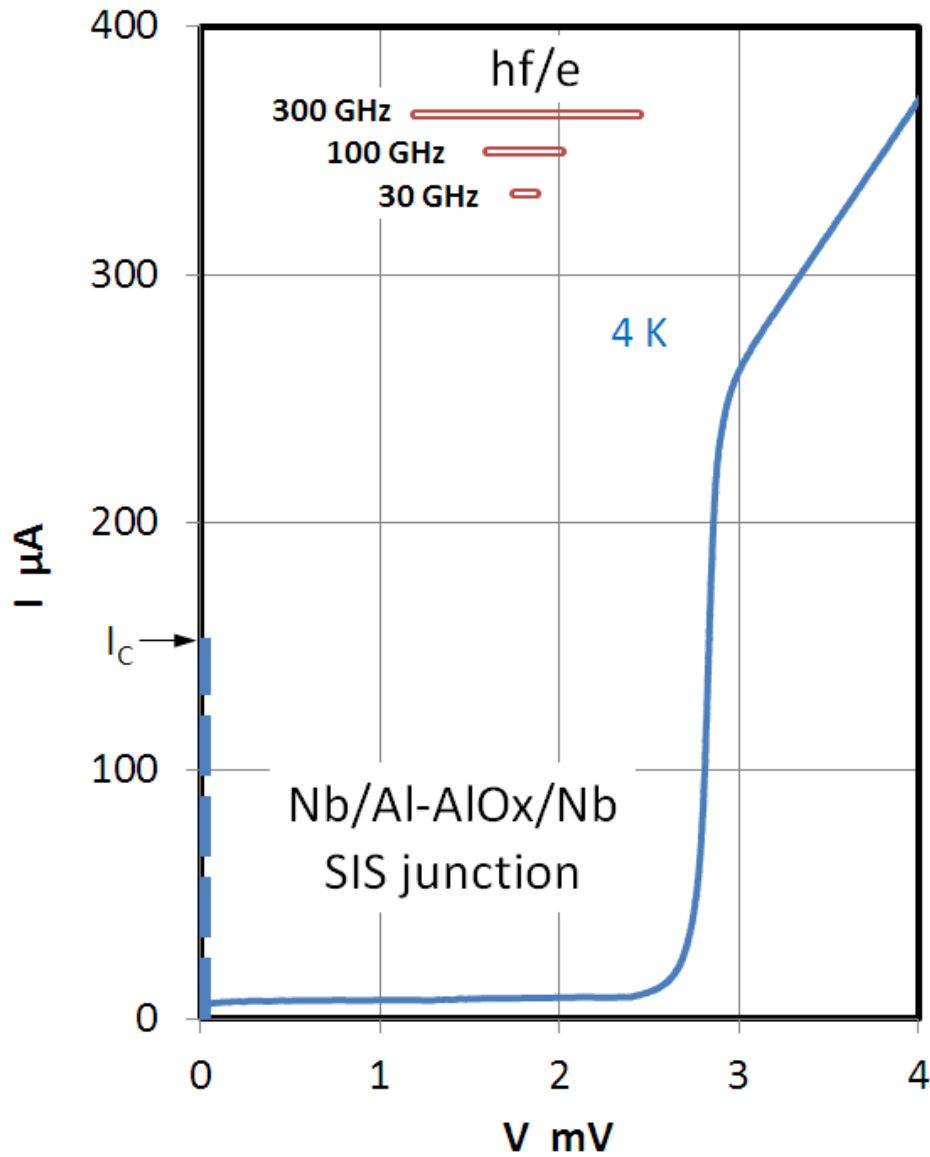
Schottky diode



Superconductor-Insulator-Superconductor (SIS) junction



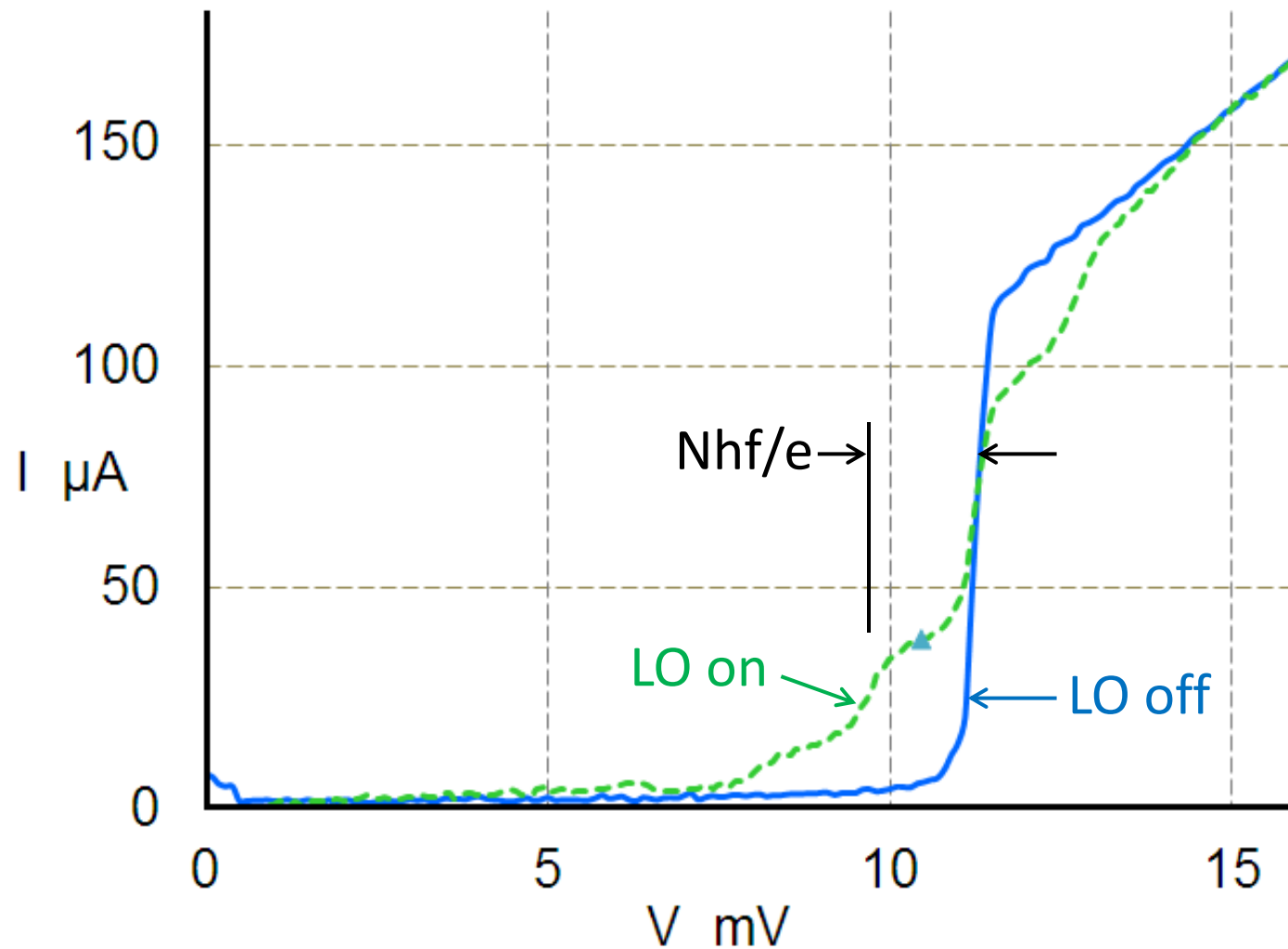
Superconductor-Insulator-Superconductor (SIS) junction



Ref. JIRMM 1990.

Photon assisted tunneling in an SIS mixer at 100 GHz.

(N = 4 junctions in series)



Classical mixer analysis

Sideband frequencies:

$$f_m = f_{IF} + mf_{LO}, \quad \text{where } f_{IF} = f_1 - f_{LO}$$

The small-signal currents and voltages at the sideband frequencies are related by the small-signal *conversion admittance matrix*, $[Y]$:

$$[I] = [Y][V]$$

For an exponential diode mixer, the elements of $[Y]$ are given by:

$$Y_{mm'} = G_{m-m'}$$

which are the Fourier coefficients of the diode conductance waveform produced by the LO.

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Tucker's quantum mixer analysis

In the quantum-limited case $Y_{mm'}$ becomes complex:

$$Y_{mm'} = G_{mm'} + jB_{mm'}$$

where

$$G_{mm'} = \frac{e}{2hf_{m'}} \sum_{n,n'=-\infty}^{\infty} J_n(\alpha) J_{n'}(\alpha) \delta_{m-m', n'-n}$$

Pumping parameter:

$$\alpha = eV_{LO}/hf_{LO}$$

$$\times \{ [I_{dc}(V_0 + n' hf_{LO}/e + hf_{m'}/e) - I_{dc}(V_0 + n' hf_{LO}/e)] \\ + [I_{dc}(V_0 + nhf_{LO}/e) - I_{dc}(V_0 + nhf_{LO}/e - hf_{m'}/e)] \}$$

$$B_{mm'} = \frac{e}{2hf_{m'}} \sum_{n,n'=-\infty}^{\infty} J_n(\alpha) J_{n'}(\alpha) \delta_{m-m', n'-n}$$

$$\times \{ [I_{KK}(V_0 + n' hf_{LO}/e + hf_{m'}/e) - I_{KK}(V_0 + n' hf_{LO}/e)] \\ - [I_{KK}(V_0 + nhf_{LO}/e) - I_{KK}(V_0 + nhf_{LO}/e - hf_{m'}/e)] \}$$

$I_{KK}(V)$ is the Kramers-Kronig transform of $I_{DC}(V)$

In the low-frequency limit, the equation for $G_{mm'}$ reduces to the classical expression on the previous slide, and $B_{mm'} \rightarrow 0$.

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Shot noise in a mixer

The shot noise currents and voltages at the sideband frequencies are related by the *noise current correlation matrix*, $[H]$.

In the classical case:

$$H_{mm'} = \langle \delta I_{S,m} \delta I_{S,m'}^* \rangle / \delta f = 2eI_{m-m'}$$

where the I_j are the Fourier coefficients of the diode current waveform produced by the LO.

Tucker's theory for the quantum-limited case:

$$H_{mm'} = e \sum_{n,n'=-\infty}^{\infty} J_n(\alpha) J_{n'}(\alpha) \delta_{m-m',n'-n} \times \{ \coth[(eV_0 + n' hf_{LO} + hf_{m'})/2kT] I_{dc} (V_0 + n' hf_{LO}/e + hf_{m'}/e) + \coth[(eV_0 + nhf_{LO} - hf_{m'})/2kT] I_{dc} (V_0 + nhf_{LO}/e - hf_{m'}/e) \}$$

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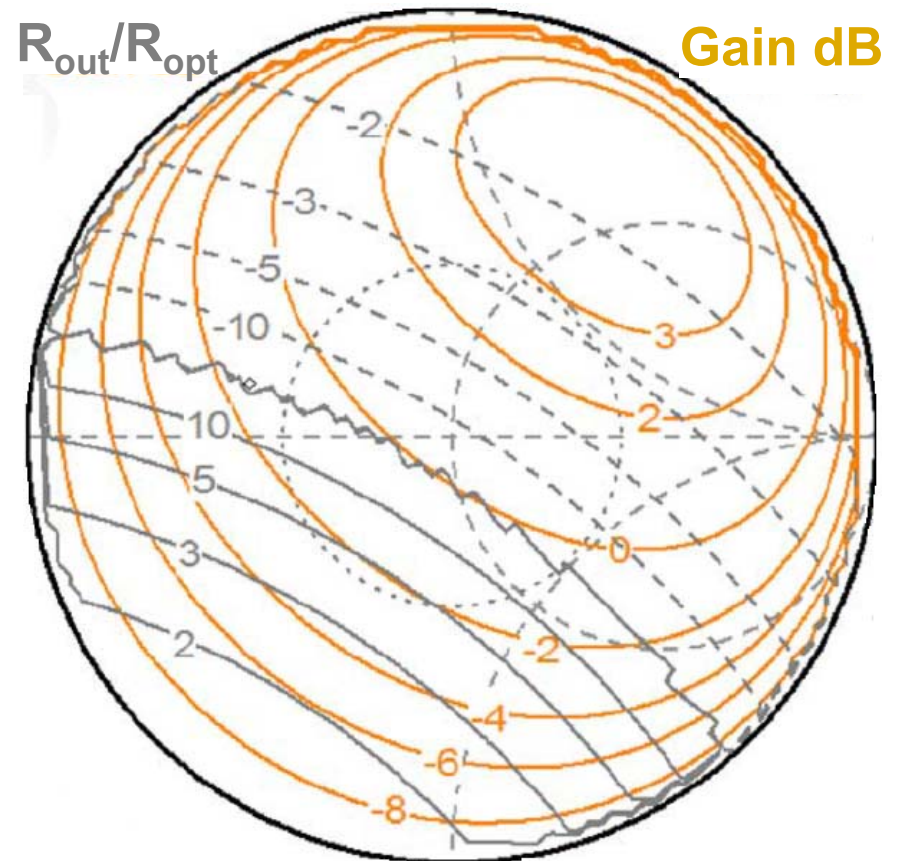
In the low-frequency limit this equation reduces to the classical expression above.

Non-classical behavior in an SIS mixer at 100 GHz.

ALMA Nb/Al-AIOx/Al SIS mixer at 100 GHz.

Contours:

- mixer gain dB.
- IF output impedance/ R_{opt}
 - dashed where negative.
 - $|\rho| = 0.4$



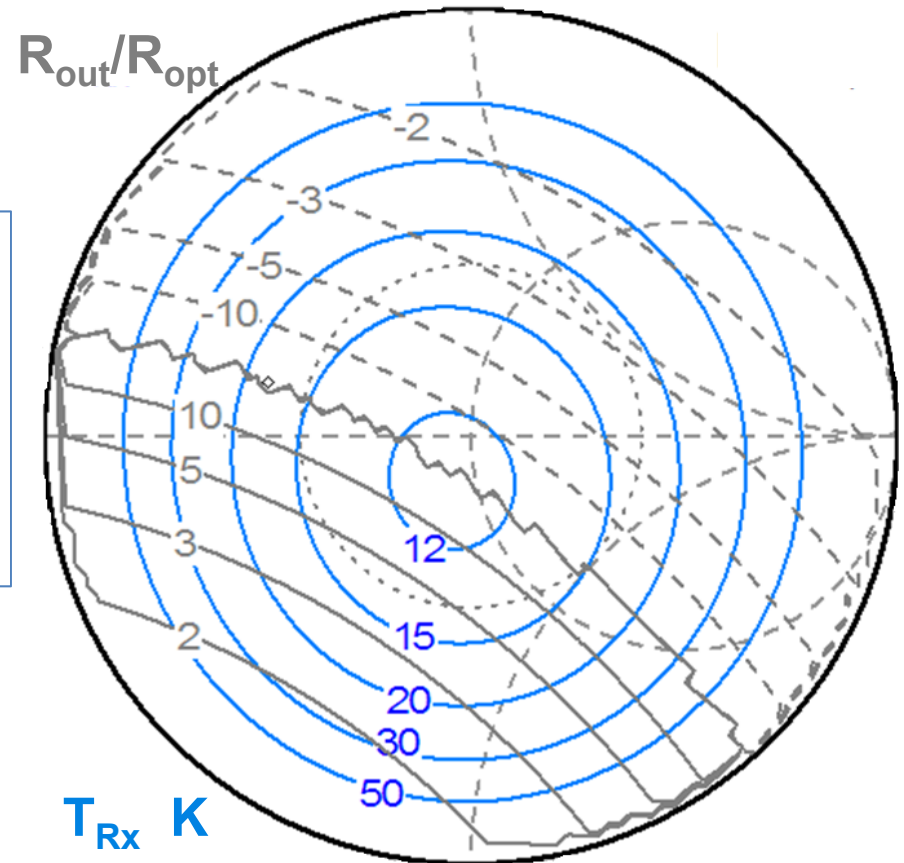
Smith chart is **RF source impedance** normalized to $Z_0 = R_{opt}$.

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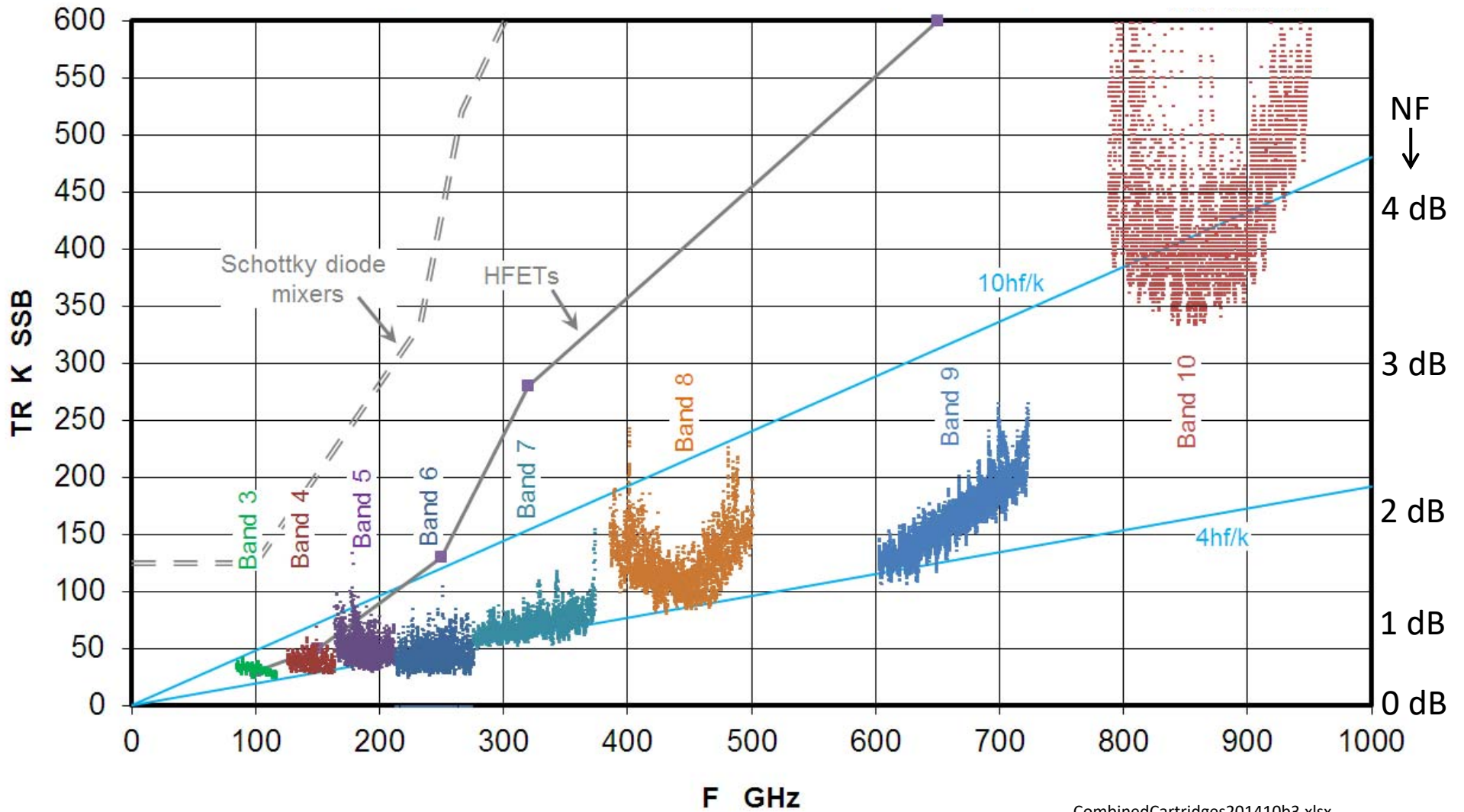
Contours:

- T_{RX} K (with $T_{IF} = 4$ K)
- IF output impedance/ R_{opt}
- dashed where negative.
- $|\rho| = 0.4$



Smith chart is **RF source impedance** normalized to $Z_0 = R_{opt}$.

Typical ALMA Receiver SSB Noise Temperatures, 2014



CombinedCartridges201410b3.xlsx



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Typical noise breakdown for an ALMA Band-6 (211-275 GHz) SIS receiver

BAND 6	L dB	T_{PHYS} K	T_N K	T_R K
Window	0.04	298	2.8	44.4
I/R filter	0.02	77	0.4	41.2
Horn + OMT	0.20	4.2	0.3	40.7
Waveguide	0.30	4.2	0.5	38.6
Image term. noise		4.2	6.6	35.6
LO Coupled noise			3.0	29.0
Mixer-Preamp			26.0	26.0

All noise temperatures are SSB.