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**5 GHZ SOURCE VARIABILITY AND THE
GAIN OF THE 300-FOOT TELESCOPE**

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ABSTRACT

During the course of the MIT-Green Bank 5 GHz survey on the NRAO 300-ft. transit telescope, about 2400 observations were made of strong sources for the purpose of calibration. In this paper we analyze the gain curve of the 300-ft. telescope between -10° and $+30^\circ$, including its time stability, and discuss the variability of the 123 calibrator sources that were observed.

I. INTRODUCTION

The MIT-Green Bank survey of 2.2 sr of sky between -0.5° and 19.5° , begun in 1979 using the NRAO* 300-ft. (91.4 m) transit telescope, is now nearly finished.

During the course of the survey repeated observations were made of 123 sources, > 1 Jy, for calibration purposes. These observations were used to determine a pointing correction, and to calibrate the gain of the 300-ft. telescope. The calibrator observations over a period of several years also allow a study of source variability. In this paper we present an analysis of the gain curves of the 300-ft. telescope between -10° and $+30^\circ$, and then present ~ 2400 measurements of the fluxes of 123 calibrators.

II. OBSERVATIONS

Sources from Table 1 of Lawrence et al. (1983) were observed in July 1979, April-May 1980, June-July 1980, January-February 1981, August 1981, September-October 1981, December 1981-February 1982, and February 1983. All of the observations were made with the beam-switched "6-25 receiver" in the "Sterling mount". The two feeds are separated by $\sim 7.6'$ on the sky, and the nominal beam width (FWHP) of each is $2.8'$. The center frequency was 4.775 GHz with a bandwidth of 580 MHz, and the integration time was 0.5 sec.

The telescope was driven in declination from South to North at six times the sidereal rate, $90''/\text{sec}$. The feeds were rotated to an angle of -12° (in the sense N through E on the sky) so that a source passing through the midpoint between the two feeds goes through the half-power point of first one feed, then the other.

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III. ANALYSIS

Calibrator scans were analyzed by cross-correlation with a model beam as described by Lawrence et al. (1983). If either of the local minima of the cross-correlation did not fall within one integration period of the expected minimum position, based on the feed model, then the scan was thrown out. This occurred only rarely. The antenna temperature was calculated from the values at the two minima.

The sources used to calibrate the gain of the 300-ft. are most of those in Table 1 of Lawrence et al. (1983) for which fluxes are listed. Source temperatures from the cross-correlations were divided by the fluxes from the table to give gain values. Several models were fitted to the gain values as a function of declination. The best fit was obtained with the following polynomial:

$$G(K/Jy) = G_0 \left[1 + \frac{G_2}{G_0} (\delta - \delta_0)^2 + \frac{G_4}{G_0} (\delta - \delta_0)^4 \right] \quad (1)$$

where $\delta_0 = 38.43^\circ$ is the declination of the zenith in Green Bank. Although this model gives a gain curve which is symmetric about the zenith, we have made observations only in the declination range $-10^\circ < \delta < 30^\circ$ and cannot comment on the accuracy of the model outside of this range.

The fit was made by reflecting the gain data points about the zenith declination, followed by a change of variables to $x_1 = (\delta_1 - \delta_0)/48.43$. Since $-1 < x_1 < 1$, Legendre polynomials could be fit to the data. Legendre polynomials are approximately orthogonal over the x_1 's and their coefficients are nearly independent. This process automatically forces the gain curve to be symmetric

about δ_0 , since the odd Legendre polynomials will vanish. The Legendre coefficients were then converted into the G_l 's of equation (1). The results are presented in Table 1 and their time variations are shown in Fig. 1. Figure 2 is representative of the high quality of all fits. The values of G_0 are significantly different for different times. The variations in $G_2/G_0 = (-5.27 \pm 0.37) \times 10^{-4}$ and in $G_4/G_0 = (7.7 \pm 1.9) \times 10^{-8}$ are insignificant. Thus the gain curve used in obtaining the fluxes in this paper is

$$G(K/Jy) = G_0(t) [1 - 5.7 \times 10^{-4} (\delta - 38.43^\circ)^2 + 7.7 \times 10^{-8} (\delta - 38.43^\circ)^4] \quad (2)$$

where $G_0(t)$ is given in Table 1.

The important result is that G_0 changes significantly over time, but G_2/G_0 and G_4/G_0 do not. In other words, the shape of the gain curve is constant, but its amplitude changes.

The antenna temperatures of ~ 2400 observations were converted into fluxes using equation (2). An editing algorithm eliminated measurements which were obviously in error, as follows: the mean flux $\langle S \rangle$, and the standard deviation of the mean, σ_m , were calculated for each source. The most extreme flux, S_E , was thrown out if

$$|S_E - \langle S \rangle| > 3 \max(\sigma_m, 0.2 \langle S \rangle). \quad (3)$$

where $\max(x,y)$ chooses the larger value of the two arguments. $\langle S \rangle$ and σ_m were recomputed, and the procedure iterated until all the measurements passed the test. Only about 25 observations ($\sim 1\%$) were thrown out, so this is a mild

TABLE I. Gain curve coefficients as a function of time. The differences in G_0 are significant. The higher order coefficients are taken as constants with values $\frac{G_2}{G_0} = (5.27 \pm 0.37) \times 10^{-4}$ and $\frac{G_4}{G_0} = (7.7 \pm 1.9) \times 10^{-8}$.

DATE	G_0	$\frac{G_2}{G_0}$	$\frac{G_4}{G_0}$
79.504	0.936	-4.86×10^{-4}	5.91×10^{-8}
80.375	1.06	-5.50	8.52
80.542	0.967	-5.22	7.86
81.125	0.943	-5.08	6.46
81.666	0.867	-5.25	7.64
81.792	0.872	-5.30	8.20
82.000	0.876	-5.03	6.36
82.375	0.855	-6.13	12.1
83.166	0.861	-5.06	6.04

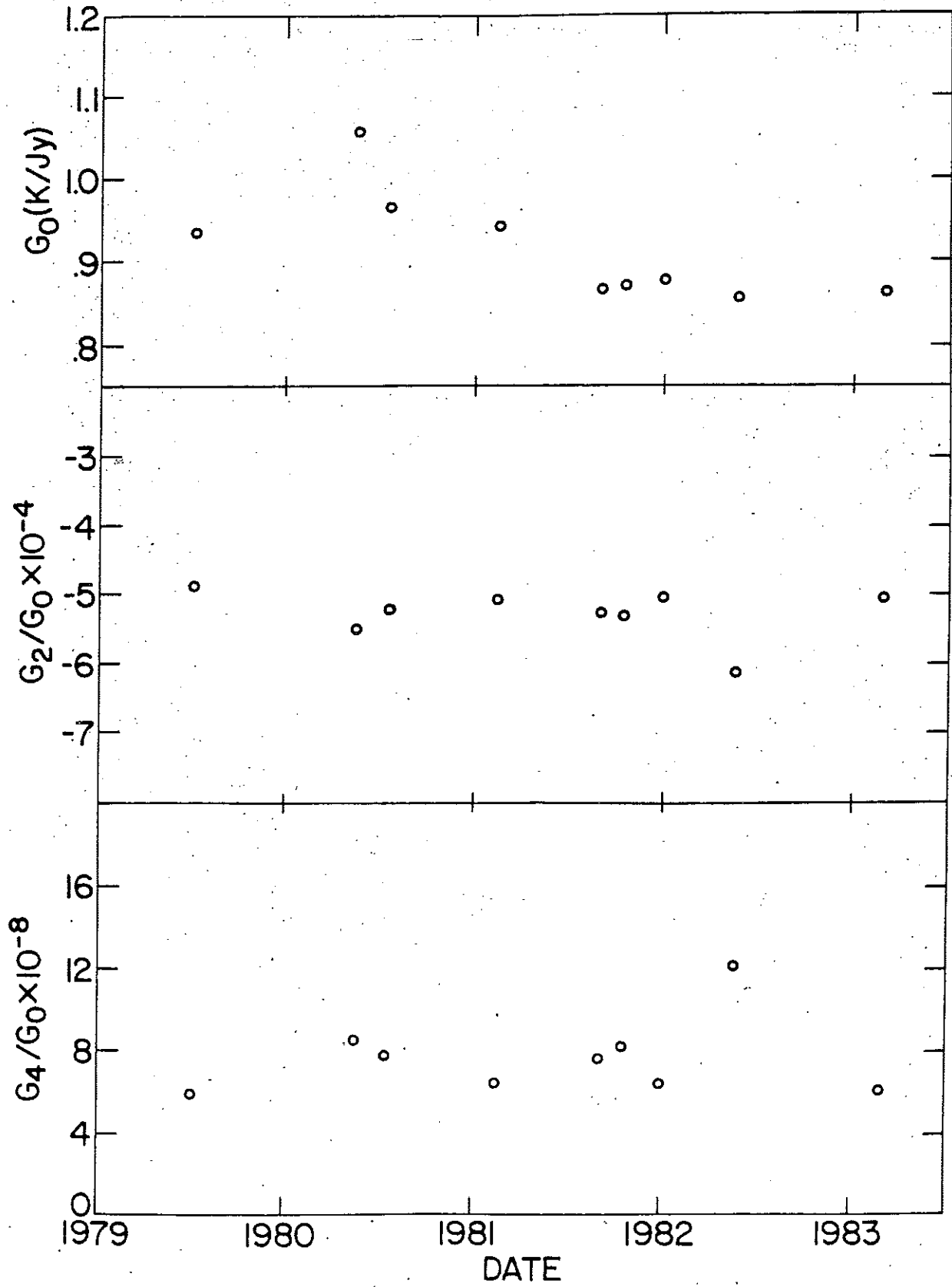


Figure 1. Gain coefficients as a function of time.

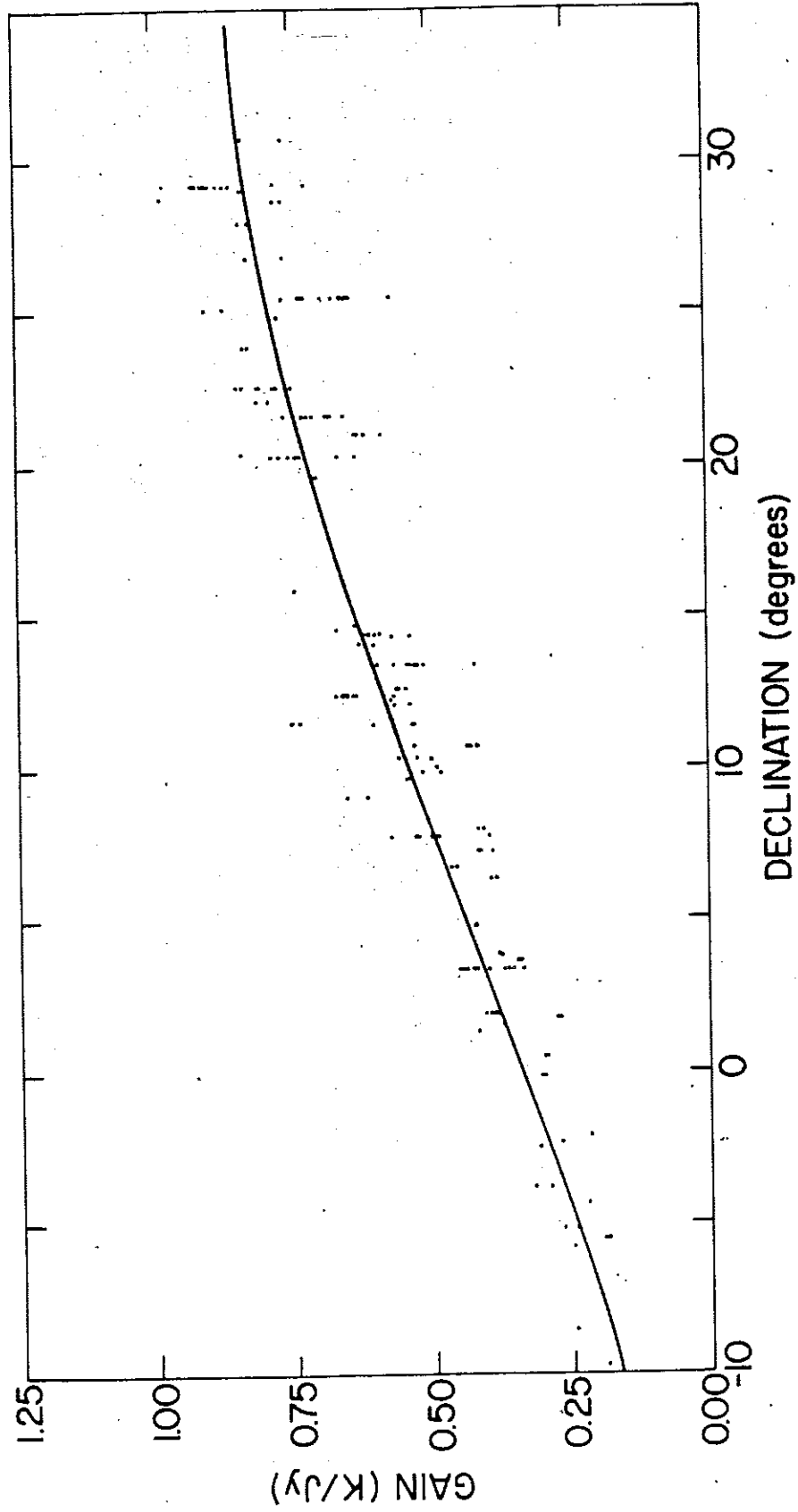


Figure 2. Gain curve fit for 1981.666 .

editing algorithm. The resulting fluxes and the corresponding dates of observation are shown in Table II. The uncertainty in a single measurement is declination dependent, but the measured dispersion for $-10^\circ < \delta < 30^\circ$ is 7.8% (Lawrence et al. 1983), as can be seen by examining measurements of a given source taken only a few days apart. The scatter is intrinsic to the 300-ft. telescope and the observing technique, as discussed by Lawrence et al. More accuracy requires redundancy and averaging.

A linear fit of the fluxes in the form

$$S(\text{year}) = A + B(\text{year}-1980) \quad (4)$$

was carried out for the individual fluxes of the sources in Table II. If a source had a flux which varied linearly with time then the coefficient A would represent the 1980 flux of the source and B would be its variability in Jy/year. The purpose of doing this fit is not to actually model the sources as varying linearly, which would more often than not be incorrect, but rather to provide the coefficient B as an indicator of variability. A source with a constant flux should have $B=0$.

A summary of the measurements is presented in Table III. Listed in the table are: the 1979 catalog flux, F, if a reliable one existed; the mean of our measured fluxes, $\langle S \rangle$; the standard deviation, σ_S ; the number of measurements, N; the coefficients A and B as described above; and the percentage deviation in the measurements $100\sigma_S/\langle S \rangle$. The reduced χ^2 of the linear fit was computed, and $100\chi/\langle S \rangle$ is listed in the table indicating the goodness of linear fit.

The fluxes of four sources are shown in Figure 3. Each is a clear example of one type of variability. 3C454.3, a well-known variable, increased steadily throughout our observations. Note in Table III that the variations about a linear fit are almost three times smaller than variations about the mean, 8.73 compared to 23.37. 3C226 remained constant, with $B=0$ in Table III, OT081, a quasar, was roughly constant until the fall of 1981, then decreased suddenly and significantly. 0736+017 is variable, but not linearly.

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REFERENCE

Lawrence, C. R., Bennett, C. L., Garcia-Barreto, J. A., Greenfield, P. E., and Burke, B. F. (1983). Astrophys. J. Suppl. 51, 67.

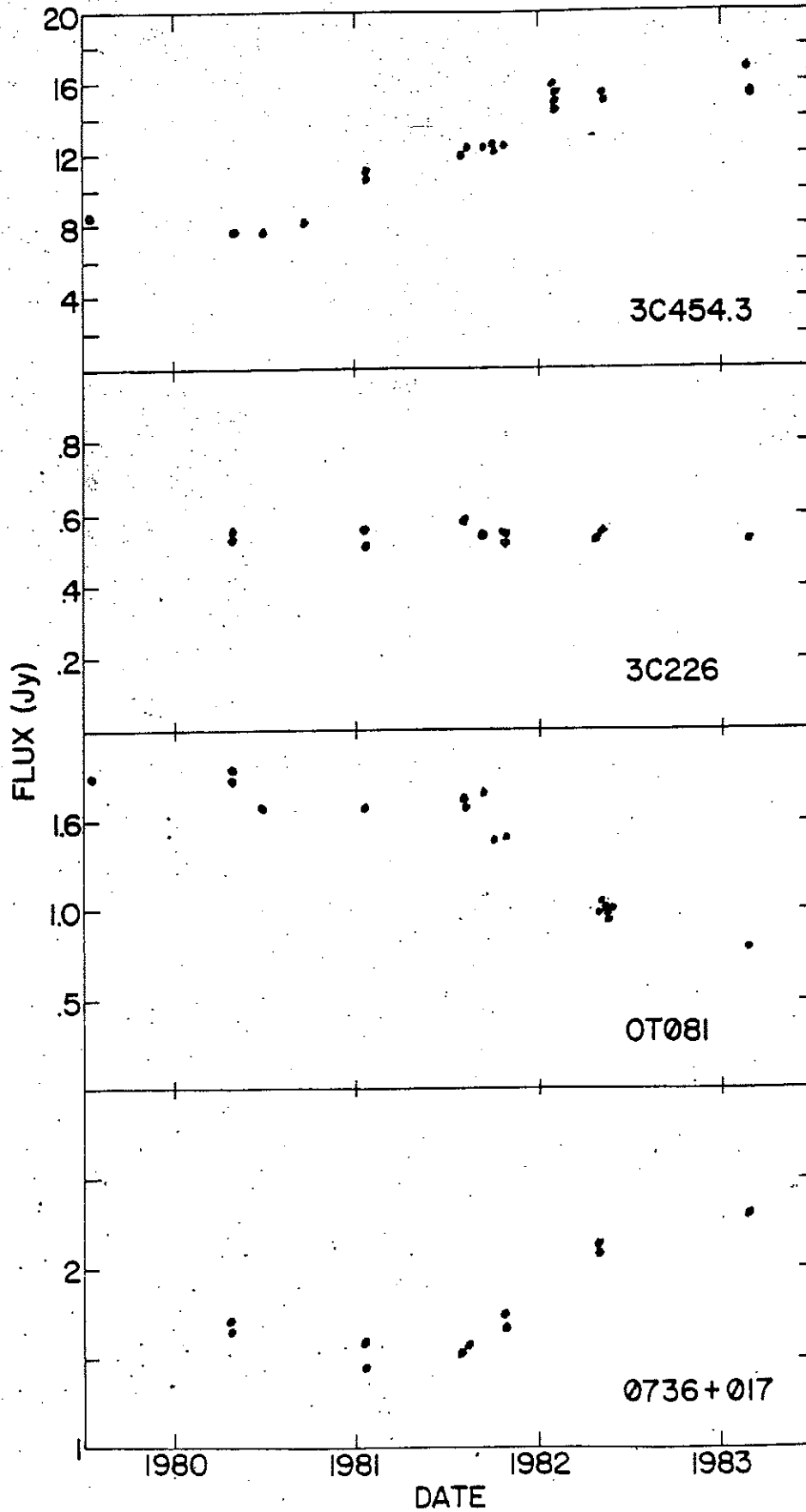


Figure 3. Fluxes of four sources. 3C454.3 is a well known variable. 3C226 remained constant. The flux of OT081 decreased suddenly. 0736+017

TABLE II. Dates and observed fluxes of 123 calibrator sources.

3C2

0106+013

NR091

0319+121

0486+121

4 26 00 1.437
 4 27 00 1.471
 6 27 00 1.441
 1 18 01 1.473
 1 19 01 1.448
 10 25 01 1.334
 1 28 02 1.504
 4 26 02 1.382

4 26 00 4.320
 4 27 00 4.367
 1 18 01 4.348
 1 19 01 4.428
 1 21 01 3.837
 8 6 01 4.208
 10 24 01 4.224
 10 25 01 4.396
 4 28 02 4.382
 4 26 02 4.239
 2 17 03 4.487

1 18 01 3.332
 1 21 01 3.142
 1 22 01 3.428
 10 25 01 3.429
 10 26 01 3.684
 1 20 02 3.497
 5 5 02 3.311
 5 7 02 3.327
 5 8 02 3.682
 5 10 02 3.054
 5 11 02 3.194
 5 12 02 3.402
 5 14 02 3.524
 5 15 02 3.454
 5 16 02 3.509
 2 24 03 3.478

4 26 00 1.159
 4 27 00 1.071
 6 27 00 1.078
 1 18 01 1.041
 1 21 01 0.985
 8 6 01 1.074
 10 25 01 1.024
 10 26 01 1.044
 4 26 02 0.977
 4 26 02 1.038
 5 5 02 0.994
 5 16 02 1.221
 2 17 03 0.926
 2 24 03 0.993

4 26 00 0.981
 4 27 00 1.158
 4 27 00 1.433
 1 20 01 1.085
 1 21 01 0.839
 10 25 01 1.078
 10 26 01 1.047
 4 26 02 0.897
 5 5 02 0.893
 5 6 02 0.938
 5 7 02 1.072
 5 8 02 0.883
 5 9 02 0.987
 5 10 02 0.794
 5 11 02 0.794
 5 12 02 0.962
 5 14 02 1.001
 5 15 02 0.949
 5 16 02 1.037
 2 17 03 0.878
 2 24 03 0.764

0007+171

4 26 00 0.962
 4 27 00 0.977
 6 27 00 0.930
 1 18 01 1.064
 1 19 01 0.964
 10 25 01 0.987
 1 28 02 0.895

0112-017

4 26 00 1.008
 4 27 00 0.979
 1 18 01 1.073
 1 19 01 1.146
 1 21 01 0.970
 6 6 01 1.155
 10 24 01 1.145
 10 25 01 1.234
 1 28 02 1.250
 4 26 02 1.194
 5 5 02 1.227
 5 7 02 1.327
 5 8 02 1.128
 5 9 02 1.209
 5 10 02 1.001
 5 11 02 1.150
 5 12 02 1.164
 5 15 02 1.157
 5 16 02 1.335
 2 17 03 1.428
 2 24 03 1.428

3C63

4 26 00 0.716
 4 27 00 0.888
 1 18 01 0.904
 1 21 01 0.719
 8 6 01 0.806
 10 25 01 0.817
 10 26 01 0.756
 1 28 02 0.859
 4 26 02 0.842
 5 5 02 0.818
 5 7 02 0.869
 5 8 02 0.818
 5 9 02 0.735
 5 10 02 0.756
 5 11 02 0.749
 5 14 02 0.742
 5 15 02 0.811
 5 16 02 0.735
 2 17 03 0.788
 2 24 03 0.870

3C89

4 26 00 0.751
 4 27 00 0.784
 6 23 00 0.756
 1 18 01 0.783
 1 21 01 0.659
 10 25 01 0.697
 10 26 01 0.678
 1 28 02 0.719
 4 26 02 0.738
 5 5 02 0.727
 5 7 02 0.733
 5 8 02 0.701
 5 9 02 0.547
 5 10 02 0.629
 5 11 02 0.639
 5 12 02 0.758
 5 14 02 0.616
 5 15 02 0.730
 5 16 02 0.728
 2 17 03 0.628
 2 24 03 0.699

0019-000

4 26 00 1.154
 4 27 00 1.113
 6 27 00 1.064
 1 18 01 1.120
 1 19 01 1.134
 1 21 01 0.921
 8 7 01 1.008
 10 24 01 1.000
 10 25 01 1.029
 1 28 02 1.109
 4 26 02 1.052

3C42

4 26 00 0.938
 4 27 00 0.942
 1 18 01 0.836
 1 19 01 0.978
 1 21 01 0.873
 8 6 01 0.999
 10 24 01 0.761
 10 25 01 0.993
 1 28 02 0.984
 4 26 02 0.941
 5 5 02 0.986
 5 7 02 0.955
 5 8 02 0.977
 5 9 02 0.762
 5 10 02 0.937
 5 11 02 0.970
 5 12 02 0.911
 5 14 02 0.945
 5 15 02 0.945
 5 16 02 0.921
 2 24 03 1.059

0229+132

1 18 01 2.228
 1 21 01 1.946
 1 22 01 2.124
 10 25 01 2.088
 10 26 01 1.988
 1 28 02 1.937
 5 5 02 1.872
 5 7 02 2.074
 5 8 02 1.872
 5 9 02 1.922
 5 10 02 2.107
 5 11 02 2.003
 2 17 03 2.004
 2 24 03 2.095

3C99

4 26 00 2.616
 4 27 00 2.733
 6 23 00 2.580
 1 18 01 3.116
 1 21 01 2.446
 10 25 01 2.854
 10 26 01 2.542
 4 26 02 2.250
 5 5 02 2.888
 5 7 02 2.888
 5 8 02 2.773
 5 9 02 2.639
 5 10 02 2.213
 5 11 02 2.582
 5 12 02 2.763
 5 14 02 2.338
 5 15 02 2.753
 5 16 02 2.577
 2 17 03 2.244
 2 24 03 2.499

3C12

4 26 00 0.843
 4 27 00 0.852
 6 27 00 0.823
 1 18 01 0.912
 1 19 01 0.867
 1 21 01 0.867
 8 7 01 0.806
 10 24 01 0.817
 10 25 01 0.797
 1 28 02 0.849
 4 26 02 0.844

0234+285

1 21 01 2.385
 8 6 01 2.473
 10 25 01 2.578
 10 26 01 2.535
 4 26 02 2.572
 2.862
 2.511
 2.708
 2.858
 2.631
 2.212
 2.781
 2.871
 2.802
 2.671
 2.941
 3.140

3C120

4 26 00 3.954
 4 27 00 4.072
 6 23 00 4.084
 1 18 01 3.982
 1 21 01 3.246
 10 25 01 3.490
 10 26 01 3.398
 4 26 02 4.376
 4 26 02 4.231
 5 6 02 4.237
 5 13 02 3.704

3C17

4 26 00 2.553
 4 27 00 2.548
 6 27 00 2.448
 1 18 01 2.759
 1 19 01 2.644
 1 21 01 2.225
 8 7 01 2.528
 10 24 01 2.581
 10 25 01 2.507
 1 28 02 2.677
 4 26 02 2.503

3C45

4 26 00 0.849
 4 27 00 0.856
 1 18 01 0.736
 1 19 01 0.856
 8 6 01 0.881
 10 24 01 0.731
 10 25 01 0.764
 1 28 02 0.757
 4 26 02 0.986
 5 5 02 0.728
 5 7 02 0.759
 5 8 02 0.733
 5 9 02 0.664
 5 10 02 0.676
 5 11 02 0.668
 5 12 02 0.745
 5 14 02 0.698
 5 15 02 0.759
 5 16 02 0.688
 2 24 03 0.784

3C79

4 26 00 1.279
 4 27 00 0.871
 6 23 00 1.378
 1 18 01 1.492
 1 21 01 1.247
 10 25 01 1.386
 10 26 01 1.355
 1 28 02 1.383
 4 26 02 1.387
 2 17 03 1.324
 2 24 03 1.438

3C93

4 26 00 0.718
 4 27 00 0.914
 6 23 00 0.906
 1 18 01 1.012
 1 21 01 0.829
 10 25 01 0.911
 10 26 01 0.948
 4 26 02 0.998
 5 5 02 0.988
 5 7 02 0.967
 5 8 02 0.891
 5 9 02 0.859
 5 10 02 0.833
 5 11 02 0.847
 5 12 02 0.931
 5 14 02 0.891
 5 15 02 0.889
 5 16 02 0.835
 5 17 03 0.827
 2 24 03 0.878

0048-097

4 26 00 1.347
 4 27 00 1.337
 6 27 00 1.490
 1 18 01 1.412
 1 19 01 1.434
 1 21 01 1.212
 8 7 01 1.501
 10 24 01 0.977
 10 25 01 0.947
 1 28 02 1.216
 4 26 02 1.678

3C55

4 26 00 0.645
 4 27 00 0.648
 1 18 01 0.613
 1 19 01 0.611
 8 6 01 0.667
 10 24 01 0.645
 10 25 01 0.665
 1 28 02 0.661
 4 26 02 0.664
 5 5 02 0.667
 5 7 02 0.694
 5 8 02 0.698
 5 9 02 0.419
 5 10 02 0.638
 5 11 02 0.651
 5 12 02 0.653
 5 14 02 0.670
 5 15 02 0.655
 5 16 02 0.670
 2 24 03 0.719

3C79

4 26 00 1.279
 4 27 00 0.871
 6 23 00 1.378
 1 18 01 1.492
 1 21 01 1.247
 10 25 01 1.386
 10 26 01 1.355
 1 28 02 1.383
 4 26 02 1.387
 2 17 03 1.324
 2 24 03 1.438

0408+258

4 26 00 1.299
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 6 23 00 1.258
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 1 21 01 1.326
 10 25 01 1.276
 10 26 01 1.274
 4 26 02 1.325
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 5 6 02 1.343
 5 7 02 1.301
 5 8 02 1.328
 5 9 02 1.241
 5 10 02 1.203
 5 11 02 1.315
 5 12 02 1.309
 5 14 02 1.297
 5 15 02 1.342
 5 16 02 1.271
 5 17 03 1.288
 2 24 03 1.288

3C26

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 4 27 00 0.578
 6 27 00 0.578
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 1 19 01 0.545
 1 21 01 0.470
 8 7 01 0.679
 10 24 01 0.534
 10 25 01 0.558
 1 28 02 0.604
 4 26 02 0.600

3C55

4 26 00 1.279
 4 27 00 0.871
 6 23 00 1.378
 1 18 01 1.492
 1 21 01 1.247
 10 25 01 1.386
 10 26 01 1.355
 1 28 02 1.383
 4 26 02 1.387
 2 17 03 1.324
 2 24 03 1.438

0528+134

4 26 00 4.229
 4 27 00 4.157
 6 23 00 4.325
 1 18 01 4.384
 1 21 01 4.423
 10 25 01 4.259
 10 26 01 4.209
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 4 26 02 4.611
 5 6 02 4.660
 5 13 02 4.191
 2 24 03 4.335

0056-001

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 4 27 00 1.381
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 1 19 01 1.359
 1 21 01 1.181
 8 6 01 1.321
 10 24 01 1.305
 10 25 01 1.320
 1 28 02 1.310
 4 26 02 1.201

7 17 79
4 26 80
4 27 80
6 27 80
1 18 81
1 19 81
8 4 81
8 7 81
9 11 81
10 3 81
10 25 81
1 30 82
1 31 82
1 31 82
2 2 82
5 4 82
5 5 82
2 15 83
2 25 83

0.830
0.774
0.809
0.768
0.846
0.849
0.863
0.798
0.819
0.816
0.803
0.826
0.810
0.814
0.814
0.779
0.794
0.859
0.859

7 17 79
4 26 80
4 27 80
6 27 80
1 18 81
1 19 81
8 4 81
8 7 81
9 11 81
10 3 81
10 25 81
1 30 82
1 31 82
2 2 82
5 4 82
5 5 82
2 15 83
2 25 83

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0.964
1.132
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1.008
1.848
1.004
0.967
1.050
1.164
1.031
1.012
1.056
1.015
1.162
0.980

7 17 79
4 26 80
4 27 80
6 27 80
1 18 81
1 19 81
8 4 81
8 7 81
9 11 81
9 12 81
10 3 81
10 7 81
10 25 81
1 30 82
1 31 82
2 2 82
5 4 82
5 5 82
2 15 83
2 25 83

0.928
0.644
0.664
0.619
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0.942
1.351
1.351
1.299
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1.192
1.215
1.247
1.337
1.220
1.191
1.121
1.139
1.127
1.071

2210+016

7 17 79
4 26 80
4 27 80
6 27 80
1 18 81
1 19 81
8 4 81
8 7 81
9 11 81
10 3 81
10 25 81
1 30 82
1 31 82
2 2 82
5 4 82
5 5 82
2 15 83
2 25 83

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1.062
0.975

3C454.3

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4 26 80
4 27 80
6 27 80
1 18 81
1 19 81
8 4 81
8 7 81
9 11 81
10 3 81
10 25 81
1 30 82
1 31 82
2 2 82
5 4 82
5 5 82
2 15 83
2 25 83

8.474
7.759
7.752
7.712
10.751
10.998
12.138
12.395
12.476
12.545
15.807
12.661
15.841
15.126
15.447
15.257
15.278
15.102
16.767
15.481

2320+102

7 17 79
4 26 80
4 27 80
6 27 80
1 18 81
1 19 81
8 4 81
8 7 81
9 11 81
9 12 81
10 3 81
10 7 81
10 25 81
1 30 82
1 31 82
2 2 82
5 4 82
5 5 82
2 15 83
2 25 83

1.093
0.981
0.989
1.011
1.065
1.063
0.967
0.928
0.974
0.915
0.881
0.881
0.881
0.881
0.910
0.889
0.878
0.936
1.078
1.084

2216-03K

7 17 79
4 26 80
4 27 80
6 27 80
1 18 81
1 19 81
8 4 81
8 7 81
9 11 81
10 3 81
10 25 81
1 30 82
1 31 82
2 2 82
5 4 82
5 5 82
2 15 83
2 25 83

3.741
3.522
3.729
3.663
4.041
4.051
3.691
3.759
3.741
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3.516
4.306
4.627
3.503
3.834
3.699
3.826
3.826
5.554

3C456

7 17 79
4 26 80
4 27 80
6 27 80
1 18 81
1 19 81
8 4 81
8 7 81
9 11 81
9 12 81
10 3 81
10 7 81
10 25 81
1 30 82
1 31 82
2 2 82
5 4 82
5 5 82
2 15 83
2 25 83

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0.745
0.762
0.676
0.869
0.894
0.837
0.793
0.802
0.781
0.748
0.712
0.826
0.819
0.785
0.788
0.711
0.746
0.869
0.771

3C466

7 17 79
4 26 80
4 27 80
6 27 80
1 18 81
1 19 81
8 4 81
8 7 81
9 11 81
9 12 81
10 3 81
10 7 81
10 25 81
1 30 82
1 31 82
2 2 82
5 4 82
5 5 82
2 15 83
2 25 83

0.810
0.743
0.778
0.728
0.796
0.778
0.810
0.798
0.715
0.745
0.731
0.814
0.832
0.814
0.802
0.777
0.754
0.864
0.797

3C446

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4 26 80
4 27 80
6 27 80
1 18 81
1 19 81
8 4 81
8 7 81
9 11 81
10 3 81
10 25 81
1 30 82
1 31 82
2 2 82
5 4 82
5 5 82
2 15 83

3.688
3.682
3.626
3.605
4.105
4.143
3.761
4.048
3.943
3.780
3.832
4.439
4.556
3.852
3.948
3.931
4.123

3C459

7 17 79
4 26 80
4 27 80
6 27 80
1 18 81
1 19 81
8 4 81
8 7 81
9 11 81
9 12 81
10 3 81
10 7 81
10 25 81
1 30 82
1 31 82
2 2 82
5 4 82
5 5 82
2 15 83
2 25 83

1.272
1.205
1.259
1.136
1.135
1.250
1.240
1.257
1.245
1.287
1.205
1.185
1.287
1.374
1.234
1.223
1.188
1.189
1.343
1.229

2344+072

7 17 79
4 26 80
4 27 80
6 27 80
1 18 81
1 19 81
8 4 81
8 7 81
9 11 81
9 12 81
10 3 81
10 7 81
10 25 81
1 30 82
1 31 82
2 2 82
5 4 82
5 5 82
2 15 83
2 25 83

1.649
1.534
1.526
1.582
1.768
1.680
1.473
1.520
1.584
1.428
1.488
1.382
1.513
1.488
1.447
1.444
1.413
1.535
1.652
1.448

CTA102

7 17 79
4 26 80
4 27 80
6 27 80
1 18 81
1 19 81
8 4 81
8 7 81
9 11 81
10 3 81
10 25 81
1 30 82
1 31 82
2 2 82
5 4 82
5 5 82
2 15 83
2 25 83

3.341
3.692
3.954
3.723
4.548
4.034
4.129
4.216
4.240
3.880
3.829
4.039
4.702
3.632
3.823
3.839
4.234
3.763

Notes to Table III.

<u>Column</u>	<u>Description</u>
1	Source name
2	1979 catalog flux
3	Computed mean flux $\langle S \rangle$, in Jy.
4	Standard deviation σ_s , in Jy.
5	Number of observations.
6, 7	Coefficients of linear fit: $S(\text{Jy}) = A + B(\text{year} - 1980)$.
8	$100\sigma_s / \langle S \rangle$.
9	$100\chi / \langle S \rangle$.

SOURCE	F (Jy)	S (Jy)	P (Jy)	N	A (1980 Jy)	B (Jy/yr)	100θ/(S)	100X/(S)
3C2	1.41	1.44	0.070	8	1.46	-0.01	5.40	5.80
0007+171	0.93	0.94	0.031	7	0.98	-0.04	3.27	1.97
0019-000	1.05	1.07	0.067	11	1.11	-0.03	4.27	6.35
3C12	0.82	0.83	0.039	11	0.85	-0.01	4.64	4.82
3C17	2.72	2.54	0.137	11	2.52	0.01	5.41	5.68
0040-097	1.33	1.32	0.224	11	1.38	-0.05	16.89	17.63
3C26	0.61	0.58	0.098	11	0.55	0.02	9.99	10.18
0056-001	1.46	1.34	0.088	10	1.40	-0.05	6.56	6.43
0106+013	3.67	4.27	0.166	11	4.31	-0.03	3.88	4.35
0112-017	1.15	1.17	0.114	21	0.94	0.12	9.73	5.85
3C42	0.84	0.95	0.046	21	0.90	0.03	4.93	4.49
3C45	0.75	0.083	0.000	20	0.74	0.00	11.12	11.42
3C55	0.65	0.060	0.000	20	0.62	0.01	9.21	9.33
NRA091	3.41	0.176	0.000	16	3.31	0.05	5.17	5.30
3C63	1.09	0.81	0.061	20	0.87	-0.03	7.56	7.13
0229+132	2.02	0.092	0.000	15	2.08	-0.03	4.59	4.67
0234+205	2.87	0.233	0.000	17	1.98	0.34	6.74	6.20
3C79	1.32	0.163	0.000	14	1.20	0.07	12.37	11.52
CTA21	3.33	0.765	0.000	11	2.85	0.22	22.78	23.85
0319+121	1.10	1.04	0.077	14	1.10	-0.03	7.35	6.96
3C89	0.70	0.059	0.000	21	0.76	-0.03	8.41	7.93
47A26	2.73	2.65	0.236	20	2.77	-0.06	8.89	8.93
3C93	0.89	0.90	0.055	20	0.93	-0.02	6.89	6.06
0400+258	1.79	1.28	0.044	21	1.31	-0.03	3.40	3.47
0410+121	1.16	0.98	0.124	21	1.11	-0.09	13.10	10.90
0430-014	3.10	3.72	0.280	10	3.67	0.03	7.52	7.94
3C120	4.91	3.88	0.354	11	3.81	0.05	9.12	9.55
3C132	1.05	1.24	0.050	12	1.19	0.03	4.03	3.33
3C133	2.16	2.36	0.127	11	2.23	0.08	5.39	4.77
3C138	4.33	0.262	0.000	12	4.12	0.12	4.66	4.13
0528+134	2.47	4.09	0.261	11	4.71	0.07	6.87	5.38
0531+194	2.52	0.128	0.000	12	2.49	0.02	5.88	5.29
0540+165	1.03	0.045	0.000	12	1.01	0.01	4.39	4.49
0605-085	2.78	3.22	0.279	13	2.99	1.13	8.65	8.29
3C161	6.73	7.18	0.396	11	7.12	-0.02	5.58	5.87
3C165	0.81	0.026	0.000	12	0.81	0.00	3.22	3.38
3C175.1	0.56	0.60	0.028	11	0.63	-0.02	4.67	4.27
0723-008	2.13	2.83	0.053	6	2.18	-0.07	5.11	5.08
0736+017	1.77	0.275	0.000	11	1.39	0.24	15.53	10.89
0742+033	3.84	3.62	0.154	10	3.77	-0.09	4.24	4.18
3C190	0.82	0.79	0.024	15	0.88	-0.01	3.05	3.08
0820+225	1.61	1.78	0.061	20	1.72	-0.01	3.60	3.69
0823+033	1.03	1.11	0.153	21	0.74	0.23	13.81	5.81
3C207	1.44	1.27	0.121	19	1.25	0.11	9.55	9.82
0J207	2.78	2.89	0.430	20	2.19	0.44	14.86	11.83
3C215.1	0.84	0.835	0.000	22	0.87	0.03	3.84	3.84
3C221	0.44	0.54	0.018	11	0.55	0.00	3.31	3.48
3C228	1.14	1.16	0.046	11	1.15	0.01	3.43	3.59
0K290	1.33	1.14	0.152	21	1.51	-0.23	13.29	6.83
3C237	2.01	1.99	0.152	17	2.02	-0.01	7.44	7.87
1013+208	0.72	0.051	0.000	22	0.67	0.03	7.07	6.68
1022+194	0.74	0.071	0.000	35	0.74	0.00	9.64	9.78
3C245	1.39	1.46	0.088	38	1.40	0.04	6.26	6.32
1049+215	0.95	0.78	0.040	19	0.89	0.02	4.31	4.27
1055+018	2.77	2.84	0.238	33	2.99	-0.10	8.38	8.26
1138+015	0.93	0.93	0.074	25	0.96	-0.02	8.03	8.05
1148-001	1.05	1.76	0.102	30	1.78	-0.01	5.81	5.89
1155+251	0.86	0.93	0.052	45	0.98	0.02	5.66	5.63
1210+134	0.75	0.052	0.000	46	0.78	-0.02	6.95	6.90
3C272.1	2.64	0.138	0.000	46	2.66	-0.01	5.23	5.28
3C273	31.80	2.771	0.000	46	33.38	-0.92	3.71	8.27
3C275.1	0.92	0.057	0.000	42	0.90	0.01	6.15	6.20
3C279	13.55	11.57	1.975	27	10.28	0.89	17.86	16.76
1313+07	0.77	0.056	0.000	34	0.75	0.01	7.34	7.41
1318+113	0.77	0.73	0.045	33	0.73	0.00	6.12	6.21
3C280	7.41	7.30	0.259	33	7.24	0.04	3.55	3.59
1345+125	2.71	2.61	0.178	37	2.52	0.05	6.82	6.79
1354+195	1.54	1.03	0.000	35	1.57	-0.02	6.65	6.71
08208	2.93	2.68	0.099	39	2.63	0.03	3.71	3.69
3C298	1.46	1.47	0.079	29	1.50	-0.02	5.37	5.34
1434+036	1.28	1.10	0.067	37	1.10	0.00	6.07	6.18
0Q172	1.05	0.066	0.000	22	1.00	0.03	6.24	5.85
3C304	0.28	0.021	0.000	21	0.27	0.01	7.46	7.25
0R183	1.74	1.37	0.118	19	1.41	-0.03	8.61	8.66
3C317	0.87	0.77	0.048	20	0.78	-0.01	6.25	6.38
1523+033	0.68	0.64	0.038	20	0.62	-0.01	6.29	6.35
1532+016	0.66	0.049	0.000	17	0.66	0.00	7.54	7.75
1538+149	1.22	0.154	0.000	30	1.29	-0.04	12.55	12.54
3C323.1	0.92	0.78	0.033	20	0.79	-0.01	4.20	4.25
1555+001	1.23	0.80	0.128	17	0.98	-0.10	15.91	9.20
1607+268	1.58	1.55	0.069	18	1.53	-0.01	4.48	4.58
1616+063	0.86	0.78	0.035	16	0.73	-0.01	6.62	6.43
3C336	0.69	0.74	0.036	18	0.74	0.00	4.90	5.05
1629+120	0.68	0.63	0.043	18	0.66	-0.01	6.73	6.55
3C342	0.42	0.016	0.000	18	0.42	0.00	3.88	3.81
1654+053	1.27	0.183	0.000	18	1.57	-0.18	14.34	4.10
1705+018	0.64	0.056	0.000	17	0.66	-0.01	8.65	8.70
3C359	0.21	0.024	0.000	16	0.23	-0.01	11.33	10.69
07068	2.24	2.48	0.288	14	2.73	-0.17	11.61	9.71
07081	1.58	1.34	0.344	17	1.85	-0.31	25.57	12.79
1801+001	0.95	0.067	0.000	12	0.93	0.01	7.02	7.18
1821+107	1.10	0.99	0.055	17	1.06	-0.04	5.56	3.88
1829+290	1.13	1.08	0.050	17	1.08	0.00	4.66	4.81
3C390	1.39	0.895	0.000	17	1.50	-0.07	6.79	5.09
3C394	0.71	0.032	0.000	17	0.74	-0.02	4.56	3.74
0V239.7	1.34	0.114	0.000	17	1.45	-0.07	8.50	7.23
1947+079	1.64	0.88	0.447	16	0.91	-0.02	5.63	5.25
2003+025	0.93	1.39	0.046	16	0.95	-0.01	4.98	4.77
0W-015	0.87	0.81	0.043	17	0.85	-0.02	5.25	4.87
2029+121	0.61	0.112	0.000	19	0.77	-0.10	18.45	11.39
2033+18	0.33	0.020	0.000	20	0.34	0.00	5.98	6.03
3C422	3.74	0.81	0.059	15	0.86	-0.04	7.29	6.17
2049+14	0.26	0.020	0.000	15	0.28	-0.01	7.66	6.91
2113+293	1.64	1.29	0.129	17	0.93	0.08	12.35	10.70
3C433	3.74	3.58	0.160	17	3.71	-0.09	4.48	4.84
2128+048	1.97	1.88	0.097	18	1.96	-0.06	5.19	4.54
2134+004	10.47	8.09	0.484	18	9.51	-0.40	5.45	3.71
3C436	0.99	1.01	0.036	18	1.00	0.00	3.56	3.65
2148+143	0.78	0.72	0.047	18	0.74	-0.02	6.62	6.41
3C441	0.92	0.82	0.024	19	0.81	0.00	2.95	3.01
2210+016	1.02	1.02	0.065	19	1.05	-0.02	8.31	8.41
2216-038	3.91	3.91	0.561	18	3.55	0.23	12.80	11.83
3C446	3.64	3.93	0.279	17	3.68	0.17	7.09	6.12
CTA102	3.19	3.98	0.342	18	3.81	0.11	8.58	8.40
2247+140	1.03	1.05	0.061	19	1.05	0.00	5.79	5.95
3C454.3	8.69	12.61	2.946	20	7.82	2.97	23.37	6.73
3C456	0.67	0.78	0.049	20	0.77	0.01	6.23	6.29
3C459	1.36	1.24	0.063	20	1.23	0.01	5.06	5.18
2318+049	0.68	1.09	0.236	20	0.83	0.16	21.63	17.09
2328+107	0.98	0.072	0.000	20	1.01	-0.02	7.33	7.25
3C466	0.75	0.78	0.038	20	0.77	0.01	4.86	4.77
2344+092	1.53	0.098	0.000	20	1.59	-0.04	6.40	6.88

