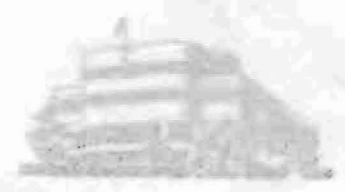
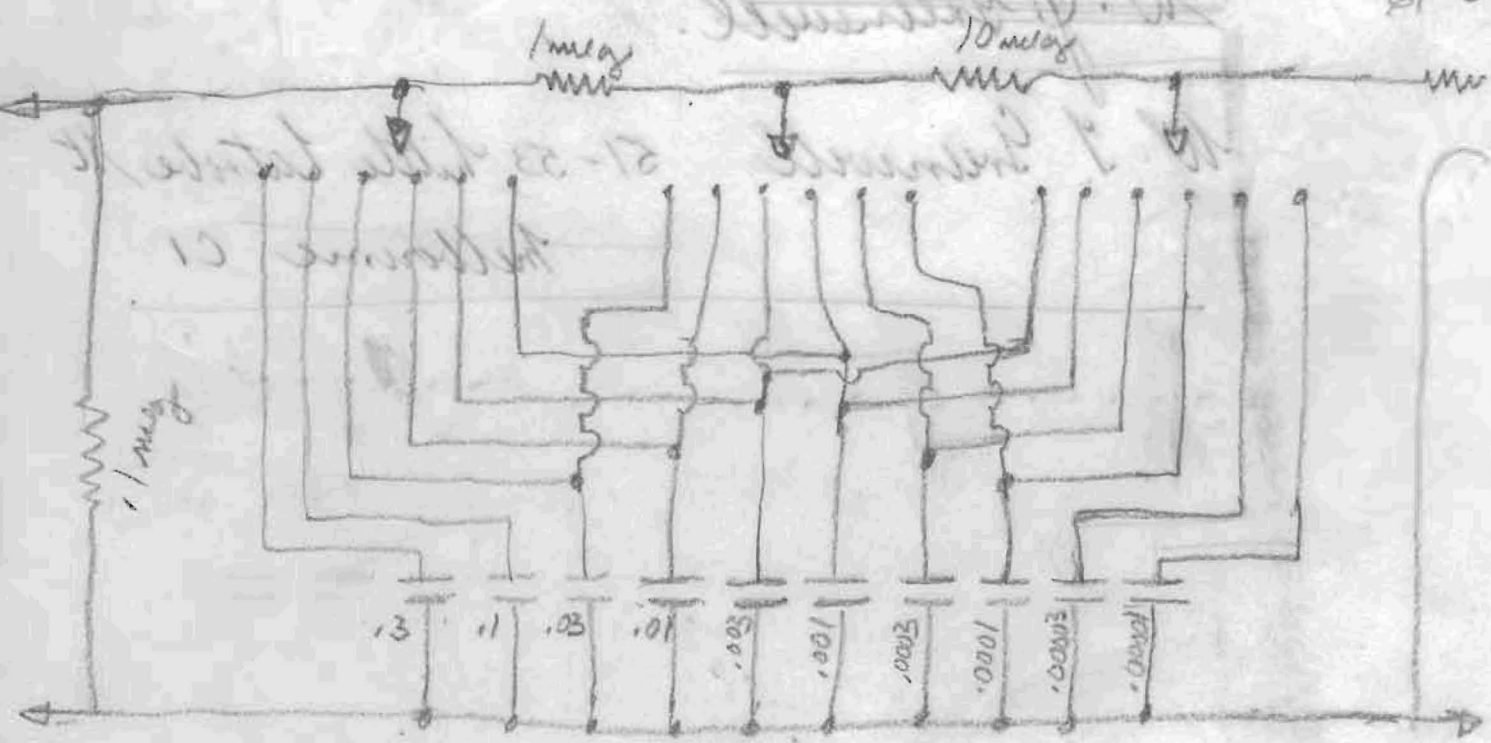


RC Time Constant	Values of R	Values of C	RC
$10^{-4}$	.001	.0001	.00001
$3 \cdot 10^{-4}$	.003	.0003	.00003
$10^{-3}$	.01	.001	.00001
$3 \cdot 10^{-3}$	.03	.003	.00003
$10^{-2}$	.1	.01	.001
$3 \cdot 10^{-2}$	.3	.03	.003



*Supplies of R & C values*

GFS





# Wrest Point Riviera Hotel

(Proprietors: Australian National Hotels Ltd.)

HOBART, TASMANIA

Suppliers of Celluloid

G Eliza Linsky 1000 640 652 Burke St.  
Melbourne CI

L. S. Williams

W. J. Greenwell

W. J. Greenwell 51-53 Little Latrobe St.  
Melbourne CI

30-8-55

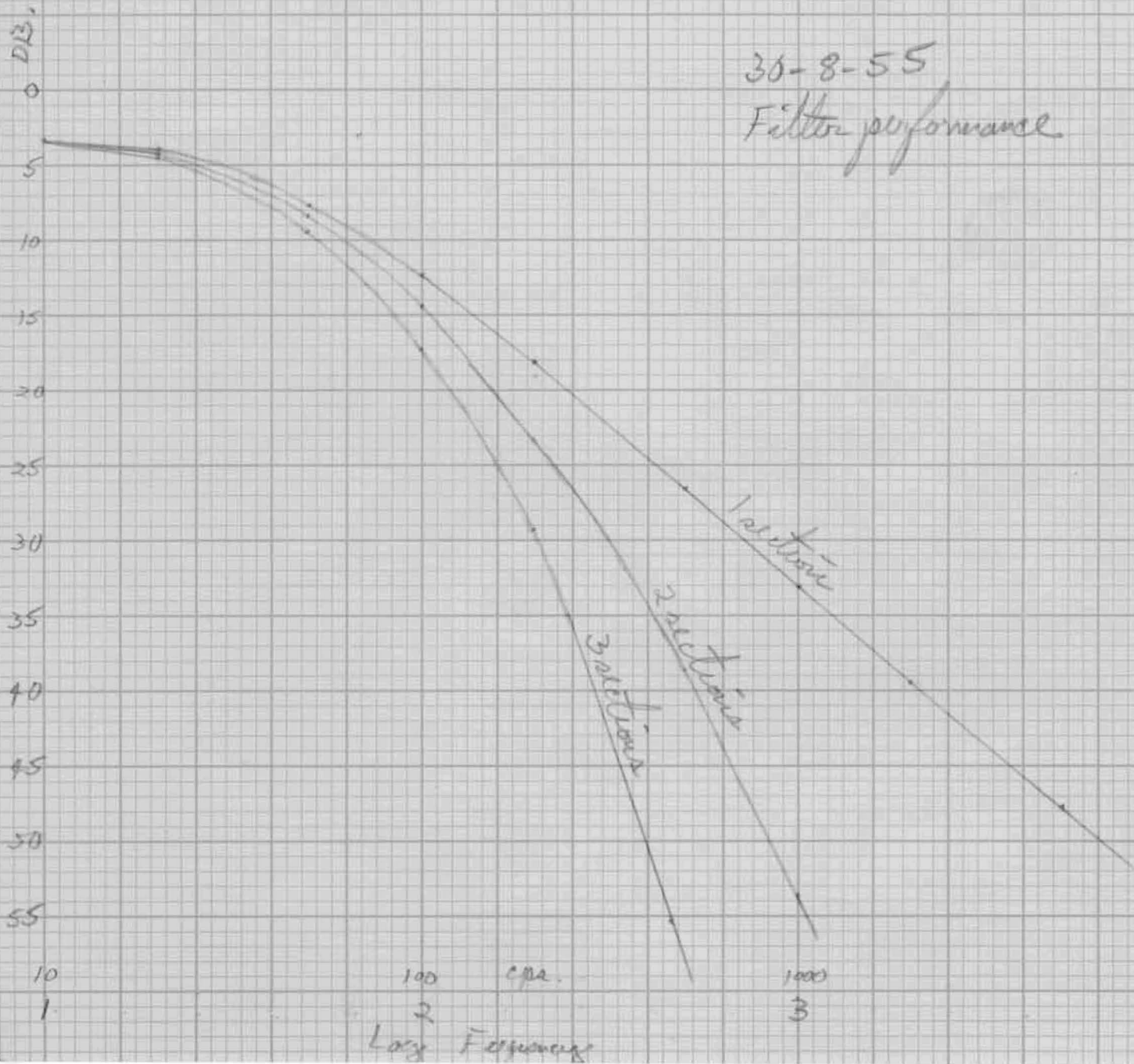
Performance of Low pass filter

6SN7 tube 1500  $\Omega$  cathode resistor,  $E_p = 150V$   $E_K = 5.1V$   
 Switch on  $10^{-3}$  seconds.  $I_p = 3.4ma$

Log. Freq.

Log. Freq.	Freq cps	1 section			2 sections			3 sections		
		Input	Output	DB	Input	Output	DB	Input	Output	DB
1.0	10	2.90	2.00	3.2	2.95	2.00	3.4	3.00	2.00	3.5
1.3	20	3.18	2.00	4.0	3.28	2.00	4.3	3.40	2.00	4.6
1.7	50	4.78	2.00	7.6	5.2	2.00	8.3	6.00	2.00	9.5
2.0	100	8.2	2.00	12.2	10.4	2.00	14.3	14.3	2.00	17.1
2.3	200	15.8	2.00	18.0	21.8	1.50	23.2	23.2	.80	29.2
2.7	500	21.2	1.00	26.5	25.6	.30	38.6	29.0	.05	55.2
3.0	1K	22.1	.50	33.0	24.0	.05	53.6			
3.3	2K	23.4	.25	39.4						
3.75	K	27.5	.10	47.8						
4.0	10K									

Input to filter  
 Output across cathode resistor of tube.



5-4-59

Stancore A 4712

Pri 7 henry 700  $\Omega$

Sec 3 henry 325  $\Omega$

Stancore A 73 C

Pri 13.5 henry 920  $\Omega$

Sec. > 110 henry 3300  $\Omega$

(each half of sec. 33.5 henry)

If  $k=1$  then  $M = 40.5$  henries

Windings in series aiding  $L = 13.5 + 122 + 8p = 217$  henries  
 $L_1 + L_2 + 2M$

choices for surge limiter



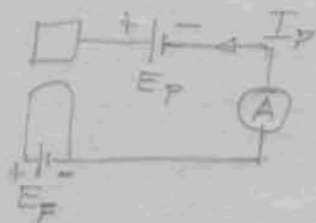
April 7, 1953

Merit Audio Trans.

	# 1	# 2
Pri. Inductance	4.2 h.	3.7 h
Pri. Resistance	440 $\Omega$	450 $\Omega$
Sec. Inductance	34 h	28 h
Sec. Resistance	1780 $\Omega$	1750 $\Omega$

14 March 1956

# Test of Diode Conductance



Meter A has 5.5  $\Omega$  on 50 ma scale  
 27  $\Omega$  " 10 ma "  
 250  $\Omega$  " 1 ma "

$E_P$ volts	0	1.5	3
Tube \ $I_P$	ma	ma	ma
1C5GT	.05	.40	2.0
1Q5GT	.9	.58	2.7
1N5GT	17	.55	1.6
1T4	.8	.36	1.6
3S4	2	.53	2.1
3E6	.05	.36	2.8

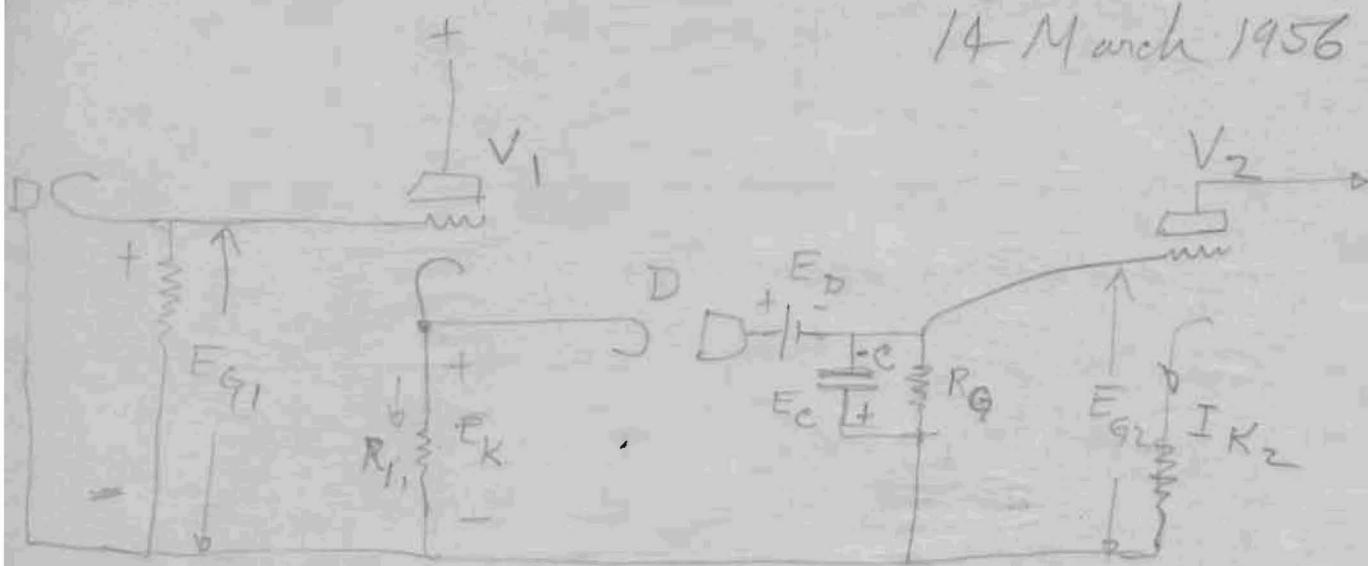
12AF	$E_P$ volts		
	5	14	21
	$I_P$ ma	ma	ma
6.6V	.20	.54	
7V	.24	.60	
8.8V	.27	.66	

3A5	26	2.4	7.0
3A5	8	1.9	5.9
3A5	26	2.2	6.8
3V4	1	.38	2.3
3V4	8	.52	2.4

$E_P$ volts	0	1.5	3
Tube \ $I_P$	ma	ma	ma
6.3V 150 ma VR92 or CV 1092, 10E/105 $\Omega$ H. Sator V. 100V	3.5	2	3.1
	4.0	11	4.0
	4.5	22	4.6
	5.0	43	5.0
	5.5	130	5.5
	6.0	230	6.0
	6.5	340	6.4
1/2 6H6	210	1.4	3.0
Full 6H6	390	2.6	5.6
6AK5 RCA	220	5.4	16
RCA	140	4.2	10
Philips	760	9.3	22
	400	6.5	17
	40	.55	6.0
	1700	8.0	17
	270	5.1	13

The 3A5 seems to give best compromise between low filament power and high conductance. At 2.2 ma for 1.5V the internal resistance is 700  $\Omega$  approx.

14 March 1956



Normally  $E_{G1}$  large and positive due to atmospheric  
 "  $E_K$  greater than  $E_D$ , so condenser C discharges  
 and  $E_{G2} = 0$   
 "  $I_{K2}$  is large

Instantaneously  $E_{G1}$  drops  
 $E_{K1} < E_D$

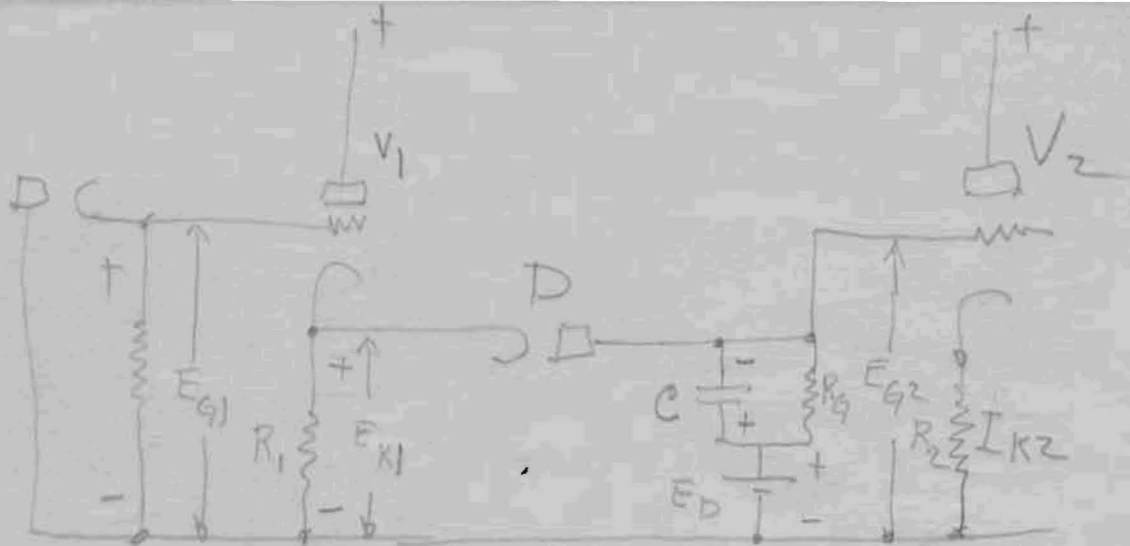
A large current flows thru diode D,  $R_1$   
 and charges C up as shown.

This provides a negative bias on  $E_{G2}$   
 which reduces  $I_{K2}$ .

Gradually C discharges,  
 $E_{G2}$  goes less negative

System depends for operation on low value of  $R_1$  and D  
 plus large value of  $R_K$ . Thus C is charged fast and  
 discharged slowly. The result is  $I_{K2}$  drops rapidly and  
 rises slowly





here situation is same in regard to  $E_{K1}$ ,  $E_D$ ,  $R_1$ ,  $D$  and  $C$ . However now  $E_D$  is in series with grid of  $V_2$  which helps hold  $E_{G2}$  near zero and thus make  $I_{K2}$  normally large. This is an advantage plus  $E_D$  does not have to be insulated from ground.

12 July 1956

# Overall Test of D.C. Amplifier

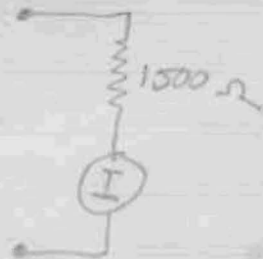
V	I	
Input Volts.	Output Current	$\Delta I$
0	0	-
1	3.5	3.5
2	7.0	3.5
3	10.9	3.9
4	14.8	3.9
5	18.2	3.4
6	21.0	2.8
7	21.3	0.3
8	21.5	0.2
9	<del>21.7</del>	-
10	21.7	0.2
12	21.9	0.2
15	22.0	0.1

Zero set range -4 to +5.4  
ma

Full scale range 19.1 to 23.8  
ma

Color	Value	Sign	Notes
gold	change	-	
Purple	38.9	-	36
white	#3	+	
	33.4	+	36
orange	#4	+	
	80.5	+	96
red	#2	+	
brown	#1	+	
	reference		

154V



grid to Grid to  
cathode, white neg.

$I_0$	Driver $E_K$	Output $E_K$	driver $E_s$	driver $E_{input}$
0	21	34	-13	+ 7.5
5	32.0	42.0	-9.9	+ 20.0
10	42.0	50.0	-7.0	+ 35.0
15	51	57	-3.0	+ 47.0
20	60	64	-1.0	+ 58.0
25	70	72	0	+ 71

Both to  
white lead

Grid to  
bottom of  
2200- $\Omega$   
resistor,  
This is  
next to  
cathode  
follower.



THE UNIVERSITY BOOKS  
ENTER BY THE  
TOOZE TEVI

356  
77

279

1698  
2082  
3780

1521  
2548  
4069

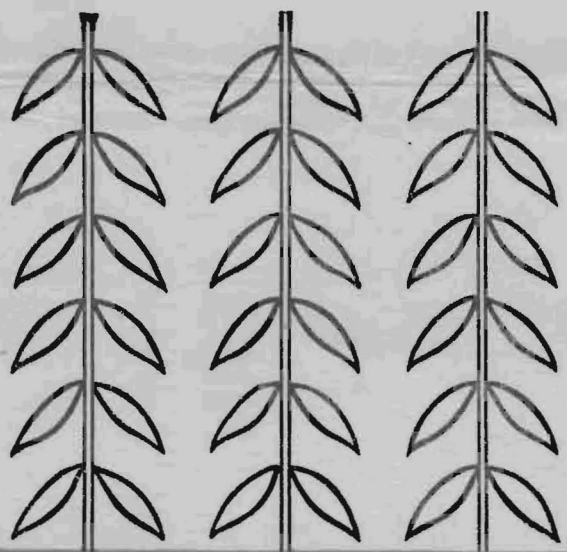
25  
256  
128  
64  
32  
16  
8

4964  
18  
4982

11000	13600	13600	11000
6000	8600	8600	6000
3200	5800	5800	3200
1600	4200	4200	1600
600	3200	3200	600
2600	2600	2600	2600

1.58  
1.44  
1.37  
1.31  
1.23

11000  
6000  
3200  
1600  
2600



4.76  
1.34  
1.05  
6.15

000121  
0006

NO. G-15964

FOR 3 RING NOTE BOOKS

**LOOSE LEAF**

**FILTER PAPER**

27/5/56

## Complete Amplifier Overall.

Clamping circuit between driver and output stages.  
 Limiter between input and driver stage.  
 Input voltage positive in relation to ground.

$$E_1 = 33.5\text{V}, E_2 = 80.0\text{V}, E_B = 113.5\text{V total.}$$

$E_K$  both in reference to negative end of  $E_B$  total.

$E_i$	$I_o$	$\Delta I_o$	$E_K$	$E_K$	$E_o$	$I_1$	$I_p$
volts	ma	ma	driver	output	volts	ma	ma
0	0	-	+19.5	+33.0	0	3.4	3.4
+2	1.1	1.1			1.7	3.5	4.6
4	2.5	1.4			3.8	3.7	6.2
6	4.0	1.5			6.0	4.0	8.0
8	5.6	1.4			8.4	4.2	9.8
10	7.1	1.5	34.5	44.0	10.8	4.4	11.5
12	9.0	1.9			13.5	4.7	13.7
14	10.8	1.8			16.2	4.9	15.7
16	12.8	2.0			19.2	5.3	18.1
18	14.6	1.8			21.9	5.5	20.1
20	16.4	1.8	53.0	57.5	24.6	5.8	22.2
22	18.2	1.8			27.3	6.1	24.3
24	20.1	1.9			30.2	6.3	26.4
26	20.5	.4			30.8	6.4	26.9
28	20.6	.1			30.9	6.4	27.0
30	20.6	0	60.5	64.0	30.9	6.4	27.0
42	20.6	0	60.5	64.0	30.9	6.4	27.0

Most of Nonlinearity at  $E_i < 8\text{V}$  is due to driver stage when its  $E_g > -11\text{V}$

(over)

Zero set range  $-2.0$  to  $+0.8$  ma

When zero set correctly

Full scale set range  $17.4$  to  $22.7$  ma

Computed time constant  $60$  Megohms  $\times$   $1$  microfarad  
is  $60$  seconds in relation to  $B+$ .

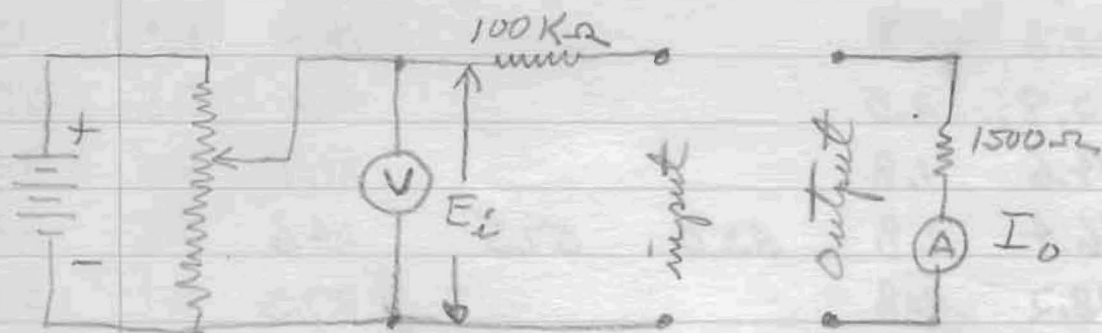
Observed time for meter hand to go from  
zero to full scale.

Fast position about  $\frac{1}{2}$  second.

Slow position nearly  $37$  seconds

$R_1 = 10,000 \Omega$ ,  $I_1 = 33.5 / 11500 = 2.9$  ma starting current.

### Test Circuit





26/5/56

## Driver and Output Stages Together.

Grid of output tied to cathode of driver. No clamping circuit between. Input direct to grid of driver stage.  $E_1 = 21.5V$ ,  $E_2 = 83.5V$ ,  $R_1 = 5000\Omega$ ,  $E_B = 105V$  total

$E_G$	$I_o$	$\Delta I_o$	$I_o$	$E_K$	$\Delta E_K$	$E_G$	$\Delta E_G$
0	26.3	-	0	8.9	-	-14.8	-
-1	24.6	1.7	5	18.9	10.0	11.1	3.7
2	22.8	1.8	10	28.4	9.5	8.1	3.0
3	20.8	2.0	15	37.9	9.5	5.5	2.6
4	19.0	1.8	20	48.1	10.2	2.9	2.6
5	16.9	2.1	25	57.0	8.9	0.5	2.4
6	15.1	1.8					
7	13.2	1.9					
8	11.6	1.6					
9	9.9	1.7					
10	8.2	1.7					
11	6.3	1.9					
12	4.8	1.5					
13	3.3	1.5					
14	1.9	1.4					
15	0.7	1.2					
16	-0.3	1.0					
17	-1.2	.9					
18	-2.0	.8					

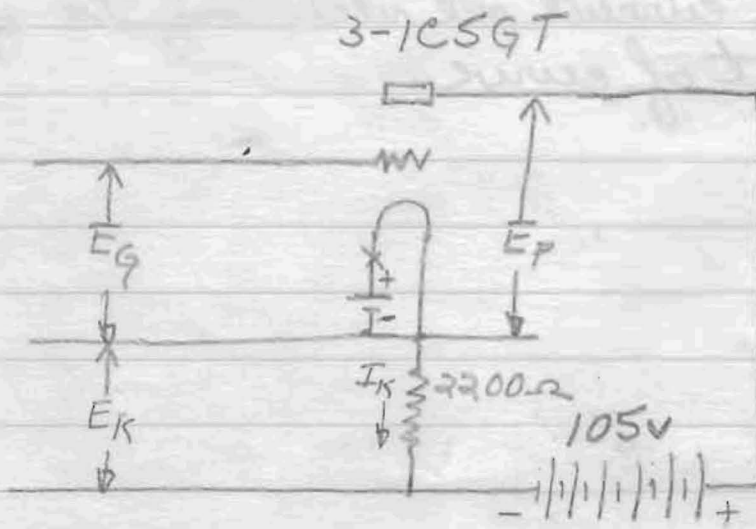
$E_G$  is voltage from driver cathode to driver grid.

$E_K$  is voltage across  $2200\Omega$  resistor in driver cathode.

When  $E_G > 11V$  the driver stage is non linear. More plate voltage or better tubes are required.

26/5/56

# Test of Triode Driver Stage



$$E_P = 105 - E_K, \quad I_K = E_K / 2200$$

$E_G$	$E_K$	$\Delta E_K$	$E_P$	$E_G$	$E_K$	$\Delta E_K$	$E_P$
0	58.0	-	47.0	11	20.2	3.3	84.8
-1	54.7	3.3	50.3	12	17.0	3.2	88.0
2	51.4	3.3	53.6	13	14.0	3.0	91.0
3	48.0	3.4	57.0	14	11.4	2.6	93.6
4	44.5	3.5	60.5	15	8.9	2.5	96.1
5	41.0	3.5	64.0	16	6.5	2.4	98.5
6	37.5	3.5	67.5	17	4.5	2.0	100.5
7	34.0	3.5	71.0	18	3.1	1.4	101.9
8	30.5	3.5	74.5	19	2.0	1.1	103.0
9	27.0	3.5	78.0	20	1.1	0.9	103.9
10	23.5	3.5	81.5				

Gain =  $\Delta E_K / \Delta E_G = 3.5 / 1.0 = 3.5 \text{ max.}$

Linear working range of  $E_K = 58.0$  to  $17.0 = 41 \text{ volts}$

This is not enough to operate output stage. A higher plate voltage is needed or other tubes

(over)

3/2/22

with a linear range nearer to cutoff. about 8ma starting current are necessary to get up on linear part of curve.



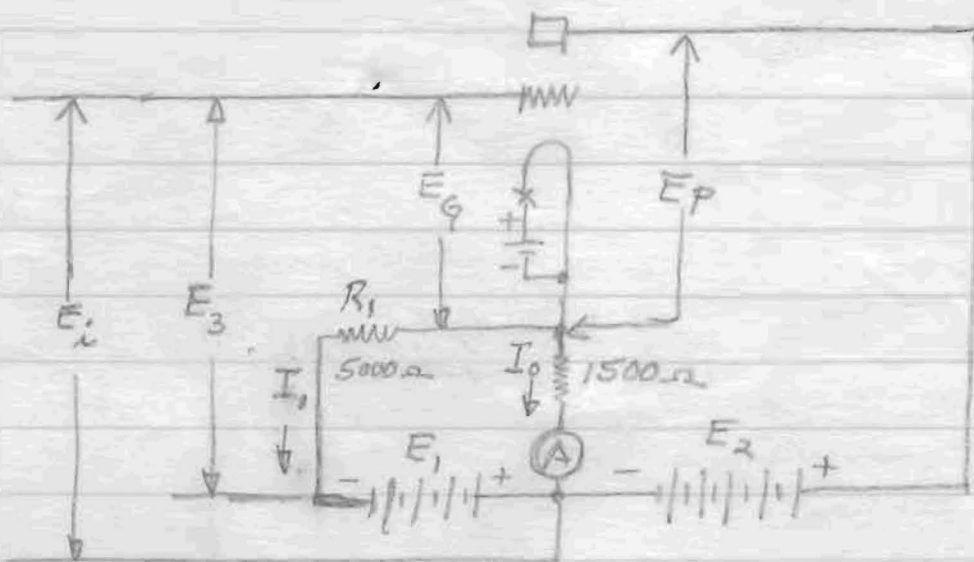
Grid - E<sub>g</sub> Plate - E<sub>p</sub>

V <sub>g</sub>	V <sub>p</sub>	I <sub>g</sub>	I <sub>p</sub>	I <sub>total</sub>
0	0	0	0	0
10	100	0.10	2.00	2.10
20	200	0.20	4.00	4.20
30	300	0.30	6.00	6.30
40	400	0.40	8.00	8.40
50	500	0.50	10.00	10.50
60	600	0.60	12.00	12.60
70	700	0.70	14.00	14.70
80	800	0.80	16.00	16.80
90	900	0.90	18.00	18.90
100	1000	1.00	20.00	21.00

29/5/56

# Test of Cathode Follower Output Stage

## 6-1C5GT



$E_1 = 41.5, E_2 = 83.5, \text{ Total } B+ = 125.0$

$E_g = E_i - E_0, E_p = E_2 - E_0, E_3 = E_1 + E_i, I_p = I_0 + I_1$

$R_L = 1 / (1/5000 + 1/1500) = 1152 \Omega, \text{ Gain} = \Delta E_0 / \Delta E_g = 3.73$

$I_1 = (E_1 + E_0) / 5000, I_0 = E_1 / 6500 = 6.4 \text{ ma starting current}$

$I_0$	$E_i$	$\Delta E_i$	$E_0$	$E_g$	$E_p$	$E_3$	$I_p$	$I_1$
ma	volts	volts	volts	volts	volts	volts	ma	(computed)

0	-12.0	-	0	-12.0	83.5	29.5	8.3	8.3
---	-------	---	---	-------	------	------	-----	-----

3	-6.0	6.0	4.5	-10.5	79.0	35.0	12.3	9.2
---	------	-----	-----	-------	------	------	------	-----

6	-0.4	5.6	9.0	-9.4	74.5	41.1	16.1	10.1
---	------	-----	-----	------	------	------	------	------

9	+5.1	5.5	13.5	-8.4	70.0	46.6	20.0	11.0
---	------	-----	------	------	------	------	------	------

12	+10.5	5.4	18.0	-7.5	65.5	52.0	23.9	11.9
----	-------	-----	------	------	------	------	------	------

15	+16.1	5.6	22.5	-6.4	61.0	57.6	27.8	12.8
----	-------	-----	------	------	------	------	------	------

18	+21.9	5.8	27.0	-5.1	56.5	63.4	31.7	13.7
----	-------	-----	------	------	------	------	------	------

21	+27.6	5.7	31.5	-3.9	52.0	69.1	35.6	14.6
----	-------	-----	------	------	------	------	------	------

24	+33.4	5.8	36.0	-2.6	47.5	74.9	39.5	15.5
----	-------	-----	------	------	------	------	------	------

Necessary working range of  $E_3 = 45.4$  volts.